

Appendix H

PRELIMINARY  
HYDROGEOLOGIC STUDY





GEOTECHNICAL ENGINEERS AND ENVIRONMENTAL CONSULTANTS

## **Preliminary Hydrogeologic Study**

**Stateline Retail Center  
East and West Disposal Areas  
Southeast, New York**

Prepared for:

Camarda Development Company  
1699 Route 6, Suite 1  
Carmel, NY 10512

Prepared by:

**GeoDesign, Inc.**  
984 Southford Road  
Middlebury, CT 06762  
Tel. (203) 758-8836  
Fax. (203) 758-8842

File No. 321-05  
December, 2006



d/b/a GeoDesign, PC

December 18, 2006  
File 321-05

Mr. Fred Koelsch  
Camarda Development Company  
1699 Route 6, Suite 1  
Carmel, NY 10512

Via: email [Fkoelsch@suscom.net](mailto:Fkoelsch@suscom.net)

Re: Preliminary Hydrogeologic Study  
Stateline Retail Center  
U.S. Route 6, Southeast NY

Dear Fred:

This report presents the results of Geo**Design**'s preliminary Hydrogeologic Study of the site of the proposed Stateline Retail Center development in the Town Southeast, New York.

### **Background Information**

Based on information provided by Insite, two areas are targeted for sewage disposal for this project. The first, the East Area, consists of an approximately 400' by 380' area near the northeast corner of the site. The second, the West area, consists on an L-shaped area approximately a 160' to 240' by 800' area (average approximately 200' by 800') located at the westerly end of the site. It is currently anticipated that in excess of 5,000 gallons per day of sewage flow will be required to service different possible development scenarios for the site. Subsurface treatment and disposal (using conventional primary sewage treatment in tank and effluent recharge into leaching trenches) is being considered.

### **Pre-Existing Subsurface Data**

Insite excavated and logged 12 deep test holes (test pits) on December 10 and 13, 2004 in a portion of the proposed East disposal area. Insite also excavated and logged about 18 deep test holes (test pits) in December, 2004 in a portion of the proposed West disposal area. Excavation depths reached to seven feet maximum in the pits. Bedrock was encountered in some of the test pits and not in others to depth of up to about 7 feet. Some bedrock outcroppings are present in portions of the site. Groundwater was not encountered at depth shallower than 6 feet. In one of the test holes a localized water seep was observed at a depth of 12 inches, but this it was not

**Preliminary Hydrogeologic Study – Stateline Retail Center**  
**December 18, 2006– File No. 321-05**  
**Page No. 2**

determined to represent groundwater. The shallow soils were generally described a “Fine Sandy Silt” or “Fine Sandy Silt and Gravel” and locally as “Fine Sand”.

### **New Subsurface Data**

Additional subsurface data was obtained in accordance with a workplan dated October 4, 2006. The purpose of the new data was to allow the preliminary estimation of the flow rate capacities of the East and the West areas in accepting subsurface sewage flow. This data was used to determine preliminary design groundwater levels and hydraulic parameters in both areas. The field investigation was performed in a manner that provided both the NYC DEP and the Putnam Dept. of Health an opportunity to review and comment on our technical approach (work plan) and witness the field testing. The intent of this approach was to help ensure that the data obtained would be acceptable to these agencies during the final site characterization phase. The final phase is scheduled to occur in future once the disposal site(s) have been chosen, once target flow rates have been selected, and at a time of the year which will allow measuring groundwater levels during the wet season (Spring or early Summer).

As described in the workplan, we engaged a subcontractor to drill 8 test borings at each area. Borings at the East and West Areas are termed BE-1 to BE-8, and BW-1 to BW-8, respectively. Drilling, testing, well installation, and well measurements occurred between October 5 and 13, 2006. A NYC DEP representative (Mr. Matt Gianetta) visited the site on the first day of drilling and testing. Subsequent groundwater observation levels were measured on October 16 and 18, 2006.

Boring logs are attached in the Appendix and boring locations are shown on Figures 1A and 1B for the East and West Areas, respectively. Each borings was terminated with a 2-inch diameter PVC observation well to allow measurement of stabilized groundwater levels. Wells were constructed with five-foot long 0.01-inch slotted screens and solid risers. Well locations and elevations (ground surface and top of riser) were surveyed by the project surveyor (Insite) and provided to us in AutoCAD format.

Borings were either extended to refusal or terminated with rock core five to ten feet below the bedrock surface. A summary of bedrock data is included in Table No. 2. We performed in-situ permeability tests below groundwater levels using the falling head methodology in unconsolidated materials in selected borings to estimate in-situ permeability. We also performed six gradation tests of selected soil samples to confirm visual classification of representative soil samples and determine D<sub>10</sub> size. Test data sheets and results are included in the Appendix.

We measured several sets of stabilized groundwater levels in all of the wells. This data is summarized in Table No. 1, attached. The phreatic (groundwater) surface levels as measured on

October 18, 2006 are also depicted on Figures 1A and 1B. Based on this data we estimated the groundwater flow gradient and direction at each proposed disposal area.

### **Calculated Permeability Estimates**

To supplement the limited field permeability testing, we performed Kozeny-Carman analyses. These analyses correlate in-situ relative density and estimated  $D_{10}$  particle size to permeability. The relative density was estimated based on standard penetration test N-values (from the test borings), and the particle size is based on the six gradation tests. The results of these data and analyses are summarized in Table 4.

### **Interpretation of Field Data and Analyses**

#### ***East Area***

About 6 to 12 inches of topsoil and subsoil are present in this area. These deposits overlie generally medium dense gravelly Sand and Silt, to depths ranging from as little as 6 feet in BE-2 to as much as 27 feet in BE-7. This stratum generally becomes denser and siltier with depth, and overlies dense Glacial Till or Gneiss Bedrock.

Depths to stabilized groundwater ranged from about 6.5 to 12.5 feet except in BE-7, near the stream where depth to water was about 1.8 foot. These readings correspond to approximate Elevations 482 to 452 decreasing toward the north. This 30 foot range in groundwater levels yields approximate hydraulic gradients of about 0.11 toward the north.

In-situ permeability test data (summarized on Table No. 3) indicated an average permeability of 1.5 feet per day. The Kozeny-Carman analyses (summarized on Table No. 4) indicate an estimated permeability of about 2.2 feet per day. These values are consistent with each other and fall within the range of published values for the gravelly sand and silt (as determined by visual classifications and gradation tests).

#### ***West Area***

About 6 to 24 inches of topsoil and subsoil are present in this area. These deposits overlie generally medium dense Sand and Silt grading to Silt and Sand, to depths ranging from about 13 to 25 feet. This stratum generally becomes denser and siltier with depth, and grades to dense Glacial Till. It overlies Gneiss Bedrock.

Depths to stabilized groundwater ranged from about 10.5 to 25.5 feet except in BW-8 nearest the wetland where depth to water was about 5.5 feet. These readings correspond to approximate Elevations 506 to 463 decreasing toward the north. This 43 foot range in groundwater levels yields approximate hydraulic gradients of about 0.08 toward the north.

In-situ permeability test data (summarized on Table No. 3) indicated an average permeability of 0.27 foot per day. The Kozeny-Carman analyses (summarized on Table No. 4) indicate an estimated average permeability of about 0.06 foot per day. These values indicate a high degree of variability, but are consistent with medium dense silty granular soils grading to dense silty Glacial Till soils.

### **Data Comparison between East and West Areas**

Depth to bedrock is greater at the West Area than at the East Area. Thus, the thickness of unconsolidated materials is greater in the West Area than in the East Area. Depth to groundwater is generally higher at the West area than at the East Area. Saturated thicknesses of the aquifer are about 8 and 13 feet at the West Area and at the East Area, respectively.

Based on limited testing, the estimated in-situ permeability of the East Area is on the order of five to ten times higher than that of the West Area.

### **Estimated Potential for Subsurface Disposal, Conclusions, and Recommendations**

Based on the referenced data, we offer the following preliminary conclusions regarding the potential for subsurface discharge and treatment of sewage. From a hydrogeologic standpoint, in general two primary factors control the suitability of discharging sewage and/or water into the ground. One is the ability of shallow soils (near the trenches) to infiltrate water at a sufficiently high rate. The other is the ability of deeper soils/bedrock formations to convey the water without excessive mounding or breakout.

We recommend that during final design percolation testing be performed at shallow depths to investigate the shallow infiltration capacity of both the East and the West Areas.

For preliminary planning purposes, we estimated the capacity of each site to accept sewage disposal flows with no breakout. Simplified one-dimensional analyses were made. The results of these analyses are included in Figures 2A and 2B, and 3A and 3B for the East and West areas, respectively. The summary of the input flow used for these analyses is included in Table No. 5. The most important assumption made for these analyses is the design base flow (groundwater flow or recharge) present at each site (e.g. before sewage flows are applied). A design value equal to 10 inches per year was used (see Figures 2A and 3A). This value is consistent with the time of the year the wells were read and the simplified model was calibrated to (October 2006) as well as the rainfall in the prior six-month period (April 2006 to October 2006). We also compared recent precipitation data to historic values for this region using recent Danbury Airport precipitation data and historic data. Refer to Tables 6A and 6B, and the partial plot of the data in Table 6B for this comparison. The values of Hydraulic Transmissivities are also critical and were estimated using the referenced permeability data, the estimated aquifer thickness, and our



experience with the types of soils/bedrock present at the site. We note that the post-flow hydraulic transmissivities used in our analyses were increased from predicted existing values to account for the expected increased aquifer thickness as the groundwater rises after the application of sewage flows. Lastly, we note that the wells were not read during the wet season, thus additional judgment had to be used. Groundwater readings made during the Spring or early Summer will be required during final design to evaluate the effects of increased based flow during the wet season.

Based on our preliminary calculations, we estimate that the East and West Areas, will be capable of accommodation approximately 7,000 gallons per day (gpd) and 3,000 gpd, respectively. See Figures 2B and 3B.

For final design, we anticipate that a mounding analysis will be required (by the NYC DEP) using a 2-D model. This will require additional testing to provide the necessary data that will then be used in analyses and preparation of a computer model to evaluate / confirm the suitability for subsurface disposal. We expect that all of the data obtained during the present study can be directly re-used for future studies of the site.

This report is subject to the attached limitations. We are available to meet with you and or Insite to discuss these results or answer any questions you may have.

If you have any questions concerning this report please the undersigned (203-758-8836, extension 105).

Very Truly Yours,

**GeoDesign, Inc.**

*Original Signed*

Ulrich La Fosse, P.E.  
Senior Principal

Attachments: Figures  
Tables  
Boring and Wells Logs  
Gradations Testing Results  
Falling Head Test Results  
Limitations

M:\cl\321-05\report.doc

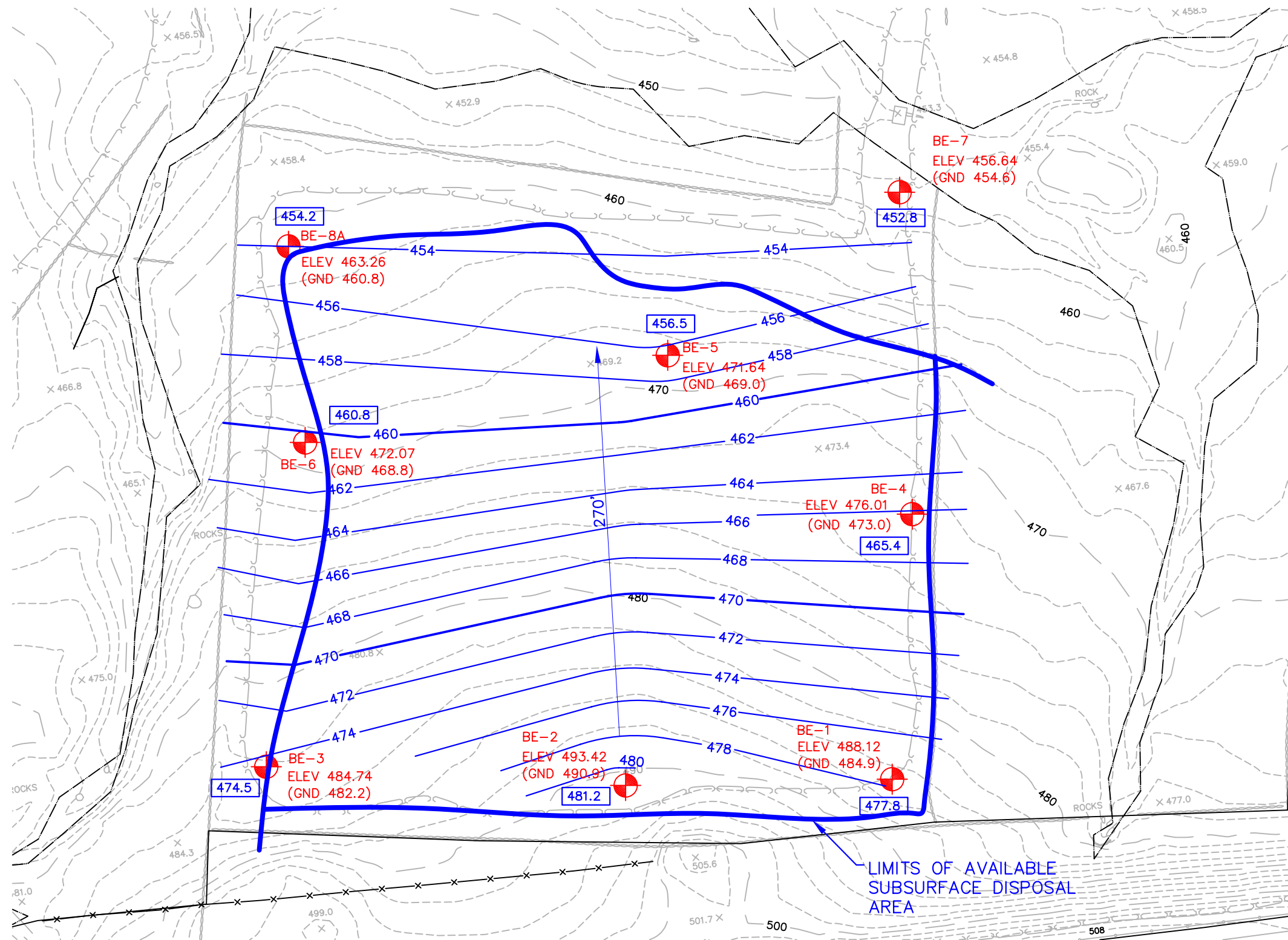


## APPENDICES



## FIGURES





- LEGEND**
- BE-1 — TEST BORING
  - ELEV. 488.12** — ELEVATION (FT)
  - (GND 484.9)** — GROUND SURFACE ELEVATION (FT)
  - 477.8** — GROUNDWATER SURFACE ELEVATION (FT) MEASURED ON 10-18-2006
  - 470** — INFERRED GROUNDWATER ELEVATION CONTOUR (FT) ON OCTOBER 18, 2006

**NOTES:**  
 1. BASEMAP PROVIDED BY INSITE VIA E-MAIL AND DATED OCT. 2006.

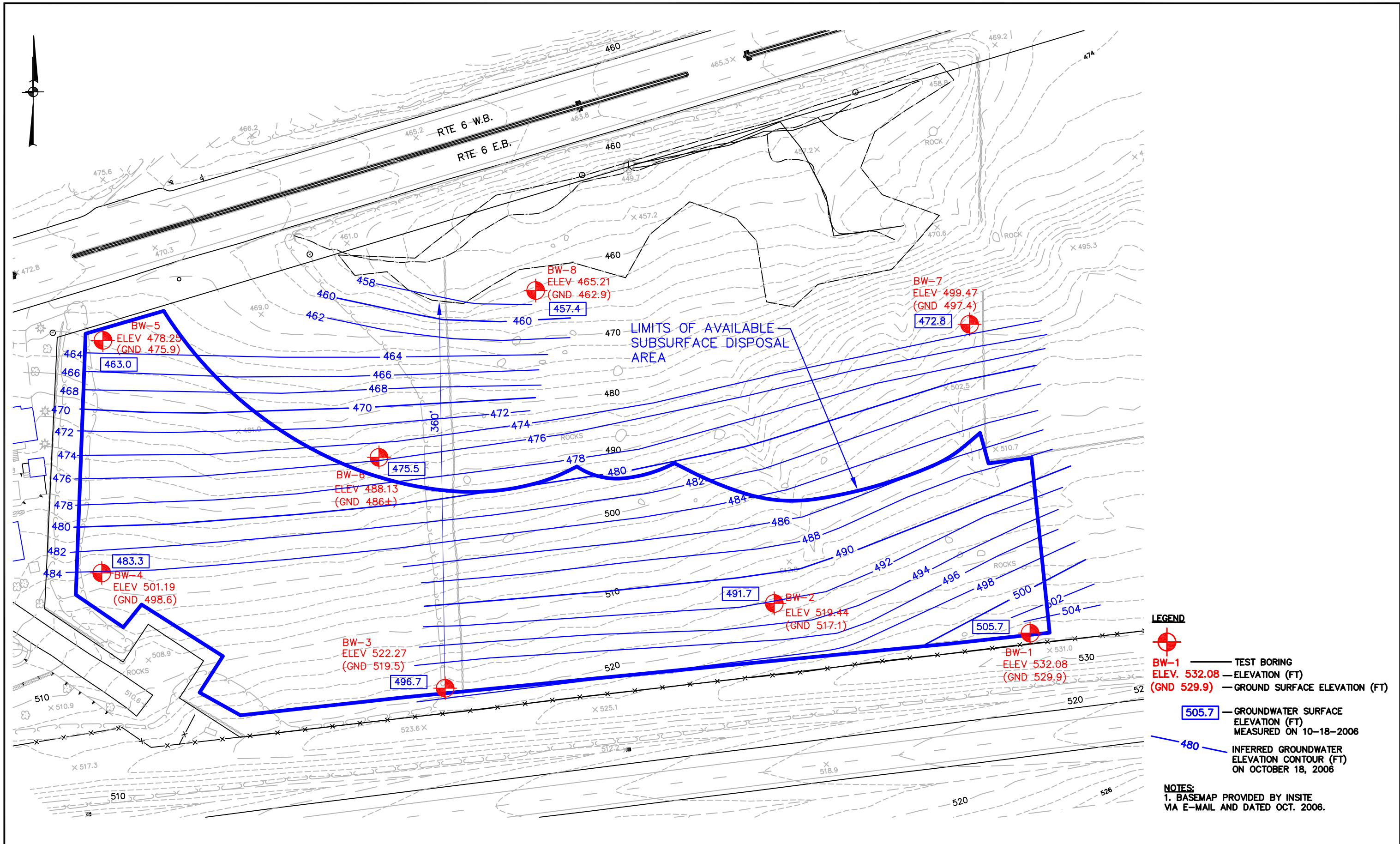
|             |           |      |       |      |       |
|-------------|-----------|------|-------|------|-------|
| DESIGNED BY |           |      |       |      |       |
| DRAWN BY    |           |      |       |      |       |
| CHECKED BY  |           |      |       |      |       |
| APPROVED BY |           |      |       |      |       |
| ULF         |           |      |       |      |       |
|             | NO.       | DATE | DRWN. | CHKD | APPVD |
|             | REVISIONS |      |       |      |       |

  
**GEODESIGN**  
 INCORPORATED  
GEOTECHNICAL ENGINEERS • ENVIRONMENTAL CONSULTANTS  
 984 SOUTHFORD ROAD • MIDDLEBURY CONNECTICUT 06762  
 TELEPHONE: (203)758-8836 FACSIMILE: (203)758-8842

|            |   |             |          |
|------------|---|-------------|----------|
| PROJECT    | STATELINE RETAIL CENTER<br>PRELIMINARY HYDROLOGICAL STUDY | FILE NO.    | 321-05   |
| SCALE      | 1" = 80'  | DATE        | 11-21-06 |
| DWG. TITLE | EAST AREA GROUNDWATER<br>ELEVATION PLAN                   | DRAWING NO. | 1A       |







- LEGEND**
- TEST BORING
  - ELEV. 532.08 — ELEVATION (FT)
  - (GND 529.9) — GROUND SURFACE ELEVATION (FT)
  - 505.7 — GROUNDWATER SURFACE ELEVATION (FT) MEASURED ON 10-18-2006
  - 480 — INFERRED GROUNDWATER ELEVATION CONTOUR (FT) ON OCTOBER 18, 2006

**NOTES:**  
 1. BASEMAP PROVIDED BY INSITE VIA E-MAIL AND DATED OCT. 2006.

|             |           |      |       |      |       |
|-------------|-----------|------|-------|------|-------|
| DESIGNED BY |           |      |       |      |       |
| DRAWN BY    |           |      |       |      |       |
| CHECKED BY  |           |      |       |      |       |
| APPROVED BY |           |      |       |      |       |
|             | NO.       | DATE | DRWN. | CHKD | APPVD |
|             | REVISIONS |      |       |      |       |

**GEODESIGN**  
INCORPORATED

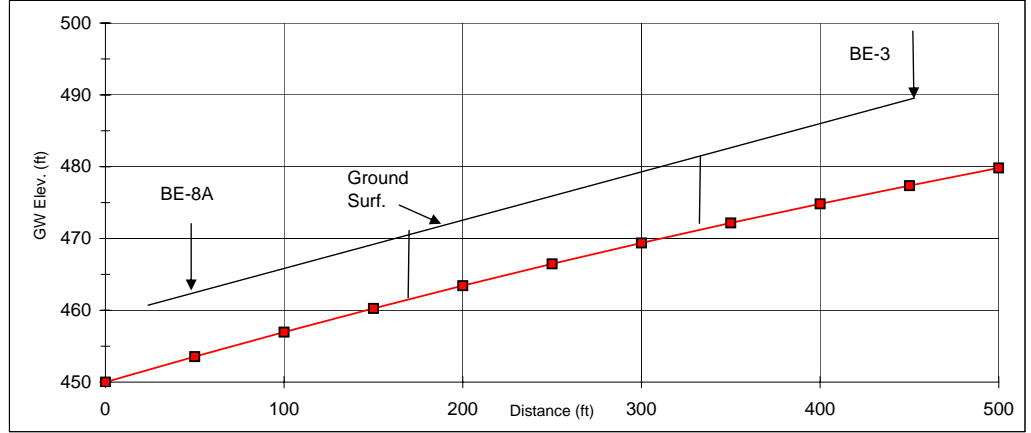
GEOTECHNICAL ENGINEERS • ENVIRONMENTAL CONSULTANTS  
 984 SOUTHFORD ROAD • MIDDLEBURY CONNECTICUT 06762  
 TELEPHONE: (203)758-8836 FACSIMILE: (203)758-8842

|            |   |             |          |
|------------|---|-------------|----------|
| PROJECT    | STATELINE RETAIL CENTER<br>PRELIMINARY HYDROLOGICAL STUDY | FILE NO.    | 321-05   |
| SCALE      | 1" = 80'  | DATE        | 11-21-06 |
| DWG. TITLE | WEST AREA GROUNDWATER<br>ELEVATION PLAN                   | DRAWING NO. | 1B       |



**LINEAR (1-D) FLOW ANALYSES**

**FIGURE 2A  
STATELINE RETAIL  
EAST AREA  
CALIBRATION**



|                                     | Mult. Factor | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     |
|-------------------------------------|--------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Point Source Flows for Widths input |              |        |        |        |        |        |        |        |        |        |        |
| Input Point Source Flow, (ft**3/d)  | 1            | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 1000   |
| Point Source Flow, Q (ft**3/d)      |              | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 1000   |
| Input Recharge (in/yr)              | 10           | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 0      |
| Recharge (in/yr)                    |              | 10     | 10     | 10     | 10     | 10     | 10     | 10     | 10     | 10     | 0      |
| Input Distances (ft)                | 0            | 50     | 100    | 150    | 200    | 250    | 300    | 350    | 400    | 450    | 500    |
| Input Width (ft)                    | 450          | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      |
| Width (ft)                          |              | 450    | 450    | 450    | 450    | 450    | 450    | 450    | 450    | 450    | 450    |
| Input Transmissivity (ft**2/d)      | 45           | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   |
| Model Transmissivity (ft**2/d)      |              | 45.00  | 45.00  | 45.00  | 45.00  | 45.00  | 45.00  | 45.00  | 45.00  | 45.00  | 45.00  |
| Final Heads (ft)                    | 450          | 453.55 | 456.97 | 460.26 | 463.43 | 466.47 | 469.38 | 472.17 | 474.83 | 477.36 | 479.83 |
| 1                                   |              | 0.06   | 0.06   | 0.06   | 0.06   | 0.06   | 0.06   | 0.06   | 0.06   | 0.06   | 0.06   |
| 2                                   |              | 0.13   | 0.19   | 0.19   | 0.19   | 0.19   | 0.19   | 0.19   | 0.19   | 0.19   | 0.19   |
| 3                                   |              | 0.13   | 0.25   | 0.32   | 0.32   | 0.32   | 0.32   | 0.32   | 0.32   | 0.32   | 0.32   |
| 4                                   |              | 0.13   | 0.25   | 0.38   | 0.44   | 0.44   | 0.44   | 0.44   | 0.44   | 0.44   | 0.44   |
| 5                                   |              | 0.13   | 0.25   | 0.38   | 0.51   | 0.57   | 0.57   | 0.57   | 0.57   | 0.57   | 0.57   |
| 6                                   |              | 0.13   | 0.25   | 0.38   | 0.51   | 0.63   | 0.70   | 0.70   | 0.70   | 0.70   | 0.70   |
| 7                                   |              | 0.13   | 0.25   | 0.38   | 0.51   | 0.63   | 0.76   | 0.82   | 0.82   | 0.82   | 0.82   |
| 8                                   |              | 0.13   | 0.25   | 0.38   | 0.51   | 0.63   | 0.76   | 0.89   | 0.95   | 0.95   | 0.95   |
| 9                                   |              | 0.13   | 0.25   | 0.38   | 0.51   | 0.63   | 0.76   | 0.89   | 1.01   | 1.08   | 1.08   |
| 10                                  |              | 2.47   | 4.94   | 7.41   | 9.88   | 12.35  | 14.81  | 17.28  | 19.75  | 22.22  | 24.69  |

Note: the formula is different along the diagonal shaded locations to account for less head loss when not all of the flow causes head loss through the starting node. There is a divide by 2 term to account for this. Note formula is  $WL^{**2}/2T$  in McWhorter & Sunada p.150 see added section for constant T by PFR This is the same formula being applied to the shaded elements where the average of 1/2 the flow causes head loss through the element with recharge.

The head loss for a point source of flow is:  $Q * L/T$

The head loss over an element with distributed flow is:  $q*L^{**2}/(2*T)$

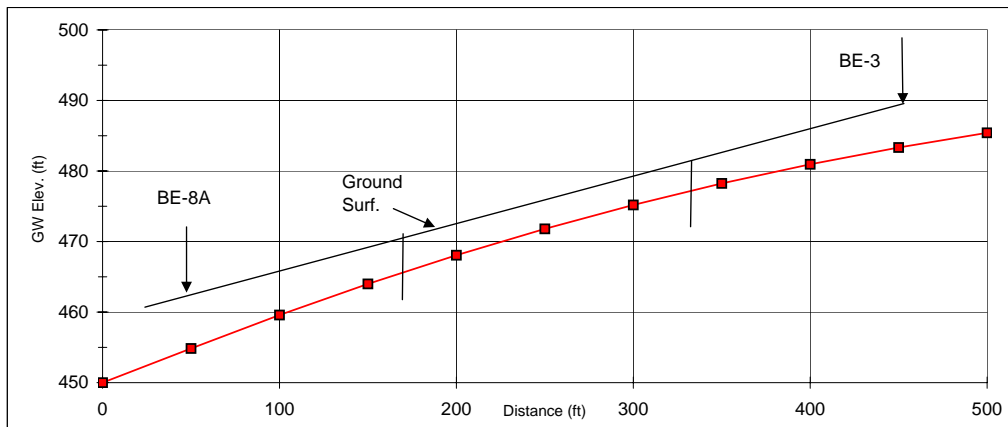
The head loss over an element that is downgradient of a distributed flow element is treated like head loss from a point source.  $Q = q*L$  and therefore the head loss is  $Q*L/T$  or  $q*L*L/T$

Shaded head loss is the head loss through that node  
Head loss terms below the shaded node are each due to the flow originating at other upgradient nodes, each term is loss due to each upgrad. Node  
Head loss terms above the shaded node are just carried upgradient for calculating final heads.

**LINEAR (1-D) FLOW ANALYSES**

**FIGURE 2B  
STATELINE RETAIL  
EAST AREA  
PREDICTION**

ft<sup>3</sup>/cell gpd  
117 7,000



| Point Source Flows for Widths input            | Mult. Factor | 1     | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     |        |
|--|--------------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Input Point Source Flow , (ft <sup>3</sup> /d) | 1            | 0     | 117    | 117    | 117    | 117    | 117    | 117    | 117    | 117    | 1000   |        |
| Point Source Flow, Q (ft <sup>3</sup> /d)      |              | 0     | 117    | 117    | 117    | 117    | 117    | 117    | 117    | 117    | 1000   |        |
| Input Recharge (in/yr)                         | 10           | 1     | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 0      |        |
| Recharge (in/yr)                               |              | 10    | 10     | 10     | 10     | 10     | 10     | 10     | 10     | 10     | 0      |        |
| Input Distances (ft)                           | 0            | 50    | 100    | 150    | 200    | 250    | 300    | 350    | 400    | 450    | 500    |        |
| Input Width (ft)                               | 400          | 1     | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      |        |
| Width (ft)                                     |              | 400   | 400    | 400    | 400    | 400    | 400    | 400    | 400    | 400    | 400    |        |
| Input Transmissivity (ft <sup>2</sup> /d)      | 60           | 1.00  | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   |        |
| Model Transmissivity (ft <sup>2</sup> /d)      |              | 60.00 | 60.00  | 60.00  | 60.00  | 60.00  | 60.00  | 60.00  | 60.00  | 60.00  | 60.00  |        |
| Final Heads (ft)                               |              | 450   | 454.84 | 459.59 | 464.00 | 468.07 | 471.80 | 475.19 | 478.24 | 480.95 | 483.33 | 485.41 |
| 1  |              | 0.05  | 0.05   | 0.05   | 0.05   | 0.05   | 0.05   | 0.05   | 0.05   | 0.05   | 0.05   |        |
| 2  |              | 0.34  | 0.63   | 0.63   | 0.63   | 0.63   | 0.63   | 0.63   | 0.63   | 0.63   | 0.63   |        |
| 3  |              | 0.34  | 0.68   | 0.97   | 0.97   | 0.97   | 0.97   | 0.97   | 0.97   | 0.97   | 0.97   |        |
| 4  |              | 0.34  | 0.68   | 1.02   | 1.31   | 1.31   | 1.31   | 1.31   | 1.31   | 1.31   | 1.31   |        |
| 5  |              | 0.34  | 0.68   | 1.02   | 1.36   | 1.65   | 1.65   | 1.65   | 1.65   | 1.65   | 1.65   |        |
| 6  |              | 0.34  | 0.68   | 1.02   | 1.36   | 1.69   | 1.99   | 1.99   | 1.99   | 1.99   | 1.99   |        |
| 7  |              | 0.34  | 0.68   | 1.02   | 1.36   | 1.69   | 2.03   | 2.32   | 2.32   | 2.32   | 2.32   |        |
| 8  |              | 0.34  | 0.68   | 1.02   | 1.36   | 1.69   | 2.03   | 2.37   | 2.66   | 2.66   | 2.66   |        |
| 9  |              | 0.34  | 0.68   | 1.02   | 1.36   | 1.69   | 2.03   | 2.37   | 2.71   | 3.00   | 3.00   |        |
| 10   |              | 2.08  | 4.17   | 6.25   | 8.33   | 10.42  | 12.50  | 14.58  | 16.67  | 18.75  | 20.83  |        |

Note: the formula is different along the diagonal shaded locations to account for less head loss when not all of the flow causes head loss through the starting node. There is a divide by 2 term to account for this. Note formula is  $WL^{**2}/2T$  in McWhorter & Sunada p.150 see added section for constant T by PFR This is the same formula being applied to the shaded elements where the average of 1/2 the flow causes head loss through the element with recharge.

The head loss for a point source of flow is:  $Q * L/T$

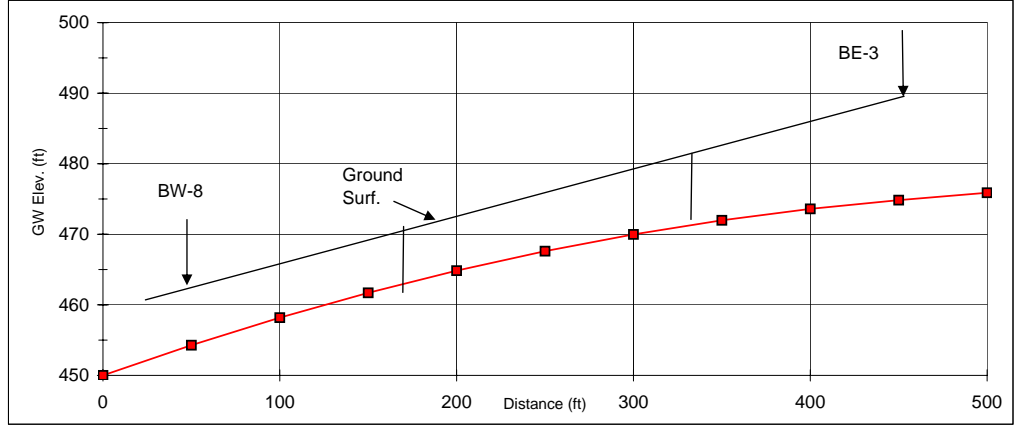
The head loss over an element with distributed flow is:  $q*L^{**2}/(2*T)$

The head loss over an element that is downgradient of a distributed flow element is treated like head loss from a point source.  $Q = q*L$  and therefore the head loss is  $Q*L/T$  or  $q*L^2/T$

Shaded head loss is the head loss through that node  
Head loss terms below the shaded node are each due to the flow originating at other upgradient nodes, each term is loss due to each upgrad. Node  
Head loss terms above the shaded node are just carried upgradient for calculating final heads.

**LINEAR (1-D) FLOW ANALYSES**

**FIGURE 3A  
STATELINE RETAIL  
WEST AREA  
CALIBRATION**



| Point Source Flows for Widths input | Mult. Factor | 1     | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     |        |
|-------------------------------------|--------------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Input Point Source Flow, (ft**3/d)  | 1            | 0     | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      |        |
| Point Source Flow, Q (ft**3/d)      |              | 0     | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 0      | 220    |        |
| Input Recharge (in/yr)              | 10           | 1     | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 0      |        |
| Recharge (in/yr)                    |              | 10    | 10     | 10     | 10     | 10     | 10     | 10     | 10     | 10     | 0      |        |
| Input Distances (ft)                | 0            | 50    | 100    | 150    | 200    | 250    | 300    | 350    | 400    | 450    | 500    |        |
| Input Width (ft)                    | 700          | 1     | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      |        |
| Width (ft)                          |              | 700   | 700    | 700    | 700    | 700    | 700    | 700    | 700    | 700    | 700    |        |
| Input Transmissivity (ft**2/d)      | 15           | 1.00  | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   |        |
| Model Transmissivity (ft**2/d)      |              | 15.00 | 15.00  | 15.00  | 15.00  | 15.00  | 15.00  | 15.00  | 15.00  | 15.00  | 15.00  |        |
| Final Heads (ft)                    |              | 450   | 454.28 | 458.18 | 461.70 | 464.84 | 467.60 | 469.98 | 471.98 | 473.60 | 474.84 | 475.89 |
| 1                                   |              | 0.19  | 0.19   | 0.19   | 0.19   | 0.19   | 0.19   | 0.19   | 0.19   | 0.19   | 0.19   |        |
| 2                                   |              | 0.38  | 0.57   | 0.57   | 0.57   | 0.57   | 0.57   | 0.57   | 0.57   | 0.57   | 0.57   |        |
| 3                                   |              | 0.38  | 0.76   | 0.95   | 0.95   | 0.95   | 0.95   | 0.95   | 0.95   | 0.95   | 0.95   |        |
| 4                                   |              | 0.38  | 0.76   | 1.14   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   | 1.33   |        |
| 5                                   |              | 0.38  | 0.76   | 1.14   | 1.52   | 1.71   | 1.71   | 1.71   | 1.71   | 1.71   | 1.71   |        |
| 6                                   |              | 0.38  | 0.76   | 1.14   | 1.52   | 1.90   | 2.09   | 2.09   | 2.09   | 2.09   | 2.09   |        |
| 7                                   |              | 0.38  | 0.76   | 1.14   | 1.52   | 1.90   | 2.28   | 2.47   | 2.47   | 2.47   | 2.47   |        |
| 8                                   |              | 0.38  | 0.76   | 1.14   | 1.52   | 1.90   | 2.28   | 2.66   | 2.85   | 2.85   | 2.85   |        |
| 9                                   |              | 0.38  | 0.76   | 1.14   | 1.52   | 1.90   | 2.28   | 2.66   | 3.04   | 3.23   | 3.23   |        |
| 10                                  |              | 1.05  | 2.10   | 3.14   | 4.19   | 5.24   | 6.29   | 7.33   | 8.38   | 9.43   | 10.48  |        |

Note: the formula is different along the diagonal shaded locations to account for less head loss when not all of the flow causes head loss through the starting node. There is a divide by 2 term to account for this. Note formula is  $WL^{**2}/2T$  in McWhorter & Sunada p.150 see added section for constant T by PFR. This is the same formula being applied to the shaded elements where the average of 1/2 the flow causes head loss through the element with recharge.

The head loss for a point source of flow is:  $Q * L/T$

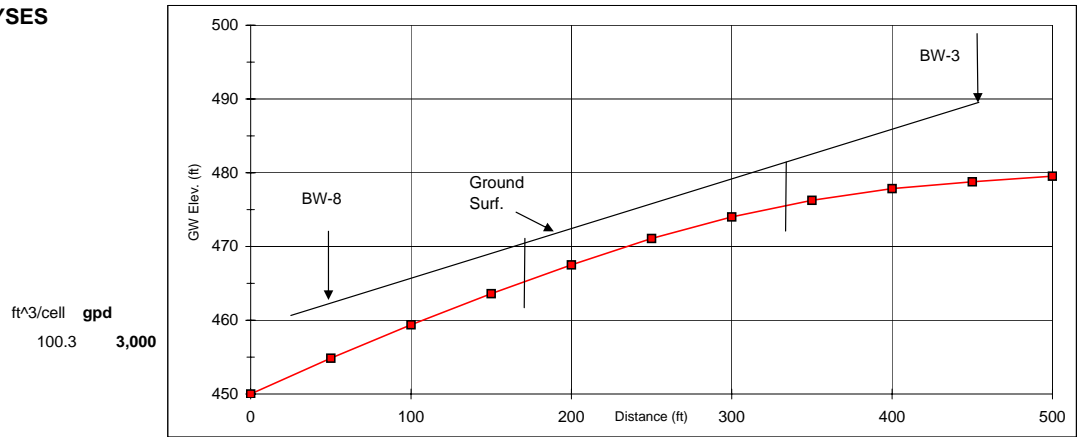
The head loss over an element with distributed flow is:  $q*L^{**2}/(2*T)$

The head loss over an element that is downgradient of a distributed flow element is treated like head loss from a point source.  $Q = q*L$  and therefore the head loss is  $Q*L/T$  or  $q*L*L/T$

Shaded head loss is the head loss through that node  
Head loss terms below the shaded node are each due to the flow originating at other upgradient nodes, each term is loss due to each upgrad. Node  
Head loss terms above the shaded node are just carried upgradient for calculating final heads.

**LINEAR (1-D) FLOW ANALYSES**

**FIGURE 3B  
STATELINE RETAIL  
WEST AREA  
PREDICTION**



| Point Source Flows for Widths input | Mult. Factor | 1     | 2      | 3      | 4      | 5      | 6      | 7      | 8      | 9      | 10     |        |
|-------------------------------------|--------------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| Input Point Source Flow, (ft**3/d)  | 1            | 0     | 0      | 0      | 0      | 100.3  | 100.3  | 100.3  | 100.3  | 0      | 220    |        |
| Point Source Flow, Q (ft**3/d)      |              | 0     | 0      | 0      | 0      | 100.3  | 100.3  | 100.3  | 100.3  | 0      | 220    |        |
| Input Recharge (in/yr)              | 10           | 1     | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 0      |        |
| Recharge (in/yr)                    |              | 10    | 10     | 10     | 10     | 10     | 10     | 10     | 10     | 10     | 0      |        |
| Input Distances (ft)                | 0            | 50    | 100    | 150    | 200    | 250    | 300    | 350    | 400    | 450    | 500    |        |
| Input Width (ft)                    | 800          | 1     | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      | 1      |        |
| Width (ft)                          |              | 800   | 800    | 800    | 800    | 800    | 800    | 800    | 800    | 800    | 800    |        |
| Input Transmissivity (ft**2/d)      | 18           | 1.00  | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   | 1.00   |        |
| Model Transmissivity (ft**2/d)      |              | 18.00 | 18.00  | 18.00  | 18.00  | 18.00  | 18.00  | 18.00  | 18.00  | 18.00  | 18.00  |        |
| Final Heads (ft)                    |              | 450   | 454.85 | 459.39 | 463.61 | 467.51 | 471.09 | 474.01 | 476.26 | 477.85 | 478.77 | 479.54 |
| 1                                   |              | 0.16  | 0.16   | 0.16   | 0.16   | 0.16   | 0.16   | 0.16   | 0.16   | 0.16   | 0.16   |        |
| 2                                   |              | 0.32  | 0.48   | 0.48   | 0.48   | 0.48   | 0.48   | 0.48   | 0.48   | 0.48   | 0.48   |        |
| 3                                   |              | 0.32  | 0.63   | 0.79   | 0.79   | 0.79   | 0.79   | 0.79   | 0.79   | 0.79   | 0.79   |        |
| 4                                   |              | 0.32  | 0.63   | 0.95   | 1.11   | 1.11   | 1.11   | 1.11   | 1.11   | 1.11   | 1.11   |        |
| 5                                   |              | 0.67  | 1.33   | 2.00   | 2.66   | 3.17   | 3.17   | 3.17   | 3.17   | 3.17   | 3.17   |        |
| 6                                   |              | 0.67  | 1.33   | 2.00   | 2.66   | 3.33   | 3.83   | 3.83   | 3.83   | 3.83   | 3.83   |        |
| 7                                   |              | 0.67  | 1.33   | 2.00   | 2.66   | 3.33   | 3.99   | 4.50   | 4.50   | 4.50   | 4.50   |        |
| 8                                   |              | 0.67  | 1.33   | 2.00   | 2.66   | 3.33   | 3.99   | 4.66   | 5.16   | 5.16   | 5.16   |        |
| 9                                   |              | 0.32  | 0.63   | 0.95   | 1.27   | 1.59   | 1.90   | 2.22   | 2.54   | 2.70   | 2.70   |        |
| 10                                  |              | 0.76  | 1.53   | 2.29   | 3.06   | 3.82   | 4.58   | 5.35   | 6.11   | 6.88   | 7.64   |        |

Note: the formula is different along the diagonal shaded locations to account for less head loss when not all of the flow causes head loss through the starting node. There is a divide by 2 term to account for this. Note formula is  $WL^2/2T$  in McWhorter & Sunada p.150 see added section for constant T by PFR This is the same formula being applied to the shaded elements where the average of 1/2 the flow causes head loss through the element with recharge.

The head loss for a point source of flow is:  $Q * L/T$

The head loss over an element with distributed flow is:  $q*L^2/(2*T)$

The head loss over an element that is downgradient of a distributed flow element is treated like head loss from a point source.  $Q = q*L$  and therefore the head loss is  $Q*L/T$  or  $q*L^2/L/T$

Shaded head loss is the head loss through that node  
Head loss terms below the shaded node are each due to the flow originating at other upgradient nodes, each term is loss due to each upgrad. Node  
Head loss terms above the shaded node are just carried upgradient for calculating final heads.

TEST BORING AND WELL LOGS







**GEODESIGN**  
 INCORPORATED  
 Geotechnical Engineers and Environmental Consultants  
 984 Southford Road  
 Middlebury, Connecticut 06762  
 Telephone: 203-758-8836 Fax: 203-758-8842



**BORING LOG**

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BE-1**  
 Page No.: **1 of 1**  
 File No.: **0321-005.0**  
 Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
 Foreman: **Jeff Leavitt**  
 GeoDesign Rep.: **Chi Zhang**  
 Date Started: **October 5, 2006** Date Finished: **October 5, 2006**  
 N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
 Ground Surface Elevation (feet): **484.0**  
 Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |            |
|--------------|--------------------|----------|--------------------------|------------|------------|------------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes      |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |            |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/5/06                  | 7.0        | 477.0      | Wet sample |
| Hammer Fall: | NA                 | 30 in.   | 10/6/06                  | 5.9        | 478.1      | In well    |
| Rig Type:    | Bombardier         |          | 10/9/06                  | 7.2        | 476.8      | In well    |
| Hammer Type: | Safety - Hydraulic |          | 10/16/06                 | 6.0        | 478.0      | In well    |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description              | Symbol   | Sample Description   |                      |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|---------------------------------|--|--|----------------------|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                                 |  |  | Moisture Content (%) |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                                 |  |  |                      |
|            | 1               | SS                 | 24   | 4                    | 0.0               | 6          | 7                       | 13     | 13      |         |                       | Sand & Gravel                   |  | Classification System: Burmister<br>Medium dense, brown fine to coarse SAND, some fine to coarse Gravel, little Silt |                      |
| 5          |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                                 |  |  |                      |
|            | 2               | SS                 | 24   | 14                   | 5.0               | 6          | 6                       | 12     | 21      |         |                       | Bottom of Exploration at 8.5 ft |  | Medium dense, brown fine to coarse SAND, some fine to coarse Gravel, little Silt                                     |                      |
| 10         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                                 |  |  |                      |
| 15         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                                 |  |  |                      |
| 20         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                                 |  |  |                      |
| 25         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                                 |  |  |                      |

Remarks: Auger refusal at 8.5 feet below grade. Moved boring 5 feet to the north and began BE-1A.

Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane;  
 WOR/H = Weight of Rod/Hammer  
 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BE-1**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**G E O D E S I G N**  
 I N C O R P O R A T E D  
 Geotechnical Engineers and Environmental Consultants  
 984 Southford Road  
 Middlebury, Connecticut 06762  
 Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BE-1A**  
 Page No.: **1 of 1**  
 File No.: **0321-005.0**  
 Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
 Foreman: **Jeff Leavitt**  
 GeoDesign Rep.: **Chi Zhang**  
 Date Started: **October 5, 2006** Date Finished: **October 5, 2006**  
 N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
 Ground Surface Elevation (feet): **484.0**  
 Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |                       |
|--------------|--------------------|----------|--------------------------|------------|------------|-----------------------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes                 |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |                       |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/5/06                  | 7.0        | 477.0      | Wet sample            |
| Hammer Fall: | NA                 | 30 in.   | 10/6/06                  | 5.9        | 478.1      | In well               |
| Rig Type:    | Bombardier         |          | 10/9/06                  | 7.2        | 476.8      | In well after 3 days  |
| Hammer Type: | Safety - Hydraulic |          | 10/16/06                 | 6.0        | 478.0      | In well after 10 days |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol | Sample Description               |  |  |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|--------|----------------------------------|--|--|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |        |                                  | Moisture Content (%)   |  |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |        |                                  |  |  |
| 5          |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                                  |  |  |
| 10         |                 | C-1                | C    | 60                   | 55                | 8.5        | [REC= 92%; RQD= 100%]   |        |         |         | 6                     |                    | 8.5    | Bedrock 475.5                    | Excellent Quality, Hard, Slightly Weathered, gray, GNEISS, moderate jointing |  |
| 15         |                 | C-2                | C    | 60                   | 60                | 13.5       | [REC= 100%; RQD= 90%]   |        |         |         | 10                    |                    | 18.5   | Bottom of Exploration at 18.5 ft | Excellent Quality, Hard, Slightly Weathered, GNEISS, moderate jointing       |  |
| 20         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                                  |  |  |
| 25         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                                  |  |  |

Remarks  
 Moved boring BE-1 five feet to the north and began BE-1A.  
 Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 10 foot screen (0.010 inch slots) and a 10 foot riser. Riser stickup is approximately 2 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

Notes:  
 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane;  
 WOR/H = Weight of Rod/Hammer  
 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BE-1A**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BE-2**  
Page No.: **1 of 2**  
File No.: **0321-005.0**  
Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
Foreman: **Jeff Leavitt**  
GeoDesign Rep.: **Chi Zhang**  
Date Started: **October 6, 2006** Date Finished: **October 6, 2006**  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): **490.0**  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/9/06                  | 10.5       | 479.5      | In well |
| Hammer Fall: | NA                 | 30 in.   | 10/10/06                 | 10.4       | 479.6      | In well |
| Rig Type:    | Bombardier         |          | 10/16/06                 | 9.8        | 480.2      | In well |
| Hammer Type: | Safety - Hydraulic |          | 10/18/06                 | 10.2       | 479.8      | In well |

| Depth (ft) | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol | Sample Description |  |                          |   |
|------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|--------|--------------------|--|--------------------------|---|
|            | Casing Blows/ft    |      | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |        |                    | Moisture Content (%)   | Depth & Elevation (feet) | Classification System: <b>Burmister</b> |
|            | Number             | Type |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |        |                    |  |                          |   |
|            | 1                  | SS   | 24                   | 16                | 0.0        | 2                       | 3      | 4       | 7       |                       |                    | 0.5    | Topsoil            | Loose, brown fine to coarse SAND and SILT, little fine to coarse Gravel, trace Roots |                          |   |
|            |                    |      |                      |                   |            |                         |        |         |         |                       |                    | 489.5  | Subsoil            |  |                          |   |
|            |                    |      |                      |                   |            |                         |        |         |         |                       |                    | 2.0    | Sand & Gravel      | Medium dense, brown fine to coarse SAND, some Silt, some fine to coarse Gravel       |                          |   |
| 5          | 2                  | SS   | 24                   | 12                | 5.0        | 6                       | 12     | 15      | 15      |                       |                    |        |                    |  |                          |   |
|            |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                    | Very dense, gray fine to coarse GRAVEL, some fine to coarse Sand, little Silt        |                          |   |
| 10         | 3                  | SS   | 14                   | 8                 | 10.0       | 18                      | 36     | 100/2"  |         |                       |                    | 11.2   | Cobbles & Boulders |  |                          |   |
|            |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                    | Excellent Quality, Moderately Hard, Slightly Weathered, gray, GNEISS                 |                          |   |
|            |                    |      |                      |                   |            |                         |        |         |         |                       |                    | 21.0   | Bedrock            |  |                          |   |
|            | C-1                | C    | 60                   | 60                | 21.0       | [REC= 100%; RQD= 90%]   |        |         |         | 6                     |                    |        |                    |  |                          |   |
| 25         |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                    |  |                          |   |

Remarks  
Auger refusal at 7 feet below grade; cored to 7.5 feet through a boulder using casing; did not get GWT.  
Cored at 11.2 feet below grade through a 4 inch diameter cobble; augered through a layer of boulders and cobbles from 11.2 to 21 feet below grade.  
Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 10 foot screen (0.010 inch slots) and a 14 foot riser. Riser stickup is approximately 2.4 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

Notes:  
1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane;  
WOR/H = Weight of Rod/Hammer  
4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BE-2**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**GEODESIGN**  
 INCORPORATED  
 Geotechnical Engineers and Environmental Consultants  
 984 Southford Road  
 Middlebury, Connecticut 06762  
 Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BE-2**  
 Page No.: **2 of 2**  
 File No.: **0321-005.0**  
 Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
 Foreman: **Jeff Leavitt**  
 GeoDesign Rep.: **Chi Zhang**  
 Date Started: **October 6, 2006** Date Finished: **October 6, 2006**  
 N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
 Ground Surface Elevation (feet): **490.0**  
 Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              |                    |          | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/9/06                  | 10.5       | 479.5      | In well |
| Hammer Fall: | NA                 | 30 in.   | 10/10/06                 | 10.4       | 479.6      | In well |
| Rig Type:    | Bombardier         |          | 10/16/06                 | 9.8        | 480.2      | In well |
| Hammer Type: | Safety - Hydraulic |          | 10/18/06                 | 10.2       | 479.8      | In well |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |                      |                         |        |         | Coring Time (min./ft) | Moisture Content (%) | Strata Description | Symbol                           | Sample Description |         |
|------------|-----------------|--------------------|------|----------------------|-------------------|----------------------|-------------------------|--------|---------|-----------------------|----------------------|--------------------|----------------------------------|--------------------|---------|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft)           | Blows / 6 inch Interval |        |         |                       |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      | 0 - 6                   | 6 - 12 | 12 - 18 |                       |                      |                    |                                  |                    | 18 - 24 |
|            |                 |                    |      |                      |                   |                      |                         |        |         | 11                    |                      |                    |                                  |                    |         |
|            | C-2             | C                  | 60   | 57                   | 26.0              | [REC= 95%; RQD= 70%] |                         |        |         | 11                    |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         | 10                    |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         | 10                    |                      |                    |                                  |                    |         |
| 30         |                 |                    |      |                      |                   |                      |                         |        |         | 12                    |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         | 7                     |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    | 31.0                             |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    | Bottom of Exploration at 31.0 ft | 459.0              |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |
| 35         |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |
| 40         |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |
| 45         |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |
|            |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |
| 50         |                 |                    |      |                      |                   |                      |                         |        |         |                       |                      |                    |                                  |                    |         |

Remarks

Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BE-2**



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name

Stateline Retail Center  
Southeast, New York

Boring No.: **BE-3**  
Page No.: **1 of 1**  
File No.: **0321-005.0**  
Checked By: **ULF**

Boring Company: New England Boring Contractors  
Foreman: Tim Carpenter  
GeoDesign Rep.: Chi Zhang  
Date Started: October 5, 2006 Date Finished: October 6, 2006  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): 483.0  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |           |
|--------------|--------------------|----------|--------------------------|------------|------------|-----------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes     |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |           |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/6/06                  | 8.8        | 474.2      | Open hole |
| Hammer Fall: | NA                 | 30 in.   | 10/9/06                  | 8.5        | 474.5      | In well   |
| Rig Type:    | Bombardier         |          | 10/10/06                 | 8.6        | 474.4      | In well   |
| Hammer Type: | Safety - Hydraulic |          | 10/18/06                 | 7.7        | 475.3      | In well   |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol   | Sample Description |   |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|--|--------------------|---|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |  |                    | Moisture Content (%)  |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |  |                    |   |
|            | 1               | SS                 | 24   | 20                   | 0.0               | 1          | 1                       | 2      | 3       |         |                       | 0.5                | Topsoil<br>Silty Sand & Gravel   | 482.5              | Very loose, brown fine to medium SAND and SILT, little fine to coarse Gravel, trace Roots |
| 5          | 2               | SS                 | 24   | 20                   | 5.0               | 4          | 4                       | 5      | 6       |         |                       | 7.0                | Loose, brown/gray fine to coarse SAND, some Silt, little fine to coarse Gravel |                    |   |
| 10         | 3               | SS                 | 24   | 20                   | 10.0              | 14         | 17                      | 17     | 19      |         |                       | 12.0               | Glacial Till   | 476.0              | Dense, gray fine to coarse SAND and fine to coarse GRAVEL, some Silt, (moist)             |
| 15         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    | Bottom of Exploration at 12.0 ft   | 471.0              |   |
| 20         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |  |                    |   |
| 25         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |  |                    |   |

Remarks: Drilled to 12 feet below grade; left hole open and taped water level next morning. Hole caved in to 9 feet. Moved 3 feet north to case a hole for falling head test. Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 5 foot screen (0.010 inch slots) and a 1.2 foot riser. Riser stickup is approximately 2.5 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

- Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BE-3**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name

**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BE-4**  
Page No.: **1 of 1**  
File No.: **0321-005.0**  
Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
Foreman: **Tim Carpenter**  
GeoDesign Rep.: **Chi Zhang**  
Date Started: **October 5, 2006** Date Finished: **October 6, 2006**  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): **473.0**  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |            |
|--------------|--------------------|----------|--------------------------|------------|------------|------------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes      |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |            |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/5/06                  | 10.0       | 463.0      | Wet sample |
| Hammer Fall: | NA                 | 30 in.   | 10/6/06                  | 9.7        | 463.3      | In well    |
| Rig Type:    | Bombardier         |          | 10/9/06                  | 8.2        | 464.8      | In well    |
| Hammer Type: | Safety - Hydraulic |          | 10/16/06                 | 6.9        | 466.1      | In well    |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         | Coring Time (min./ft) | Moisture Content (%) | Strata Description               | Symbol | Sample Description   |         |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|-----------------------|----------------------|----------------------------------|--------|--|---------|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |                       |                      |                                  |        |  |         |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 |                       |                      |                                  |        |  | 18 - 24 |
|            | 1               | SS                 | 24   | 8                    | 0.0               | 1          | 2                       | 2      | 3       |                       |                      | Topsoil                          |        | Loose, dark brown fine to coarse SAND and SILT, some fine to coarse Gravel, trace Wood |         |
| 5          | 2               | SS                 | 24   | 18                   | 5.0               | 12         | 12                      | 11     | 13      |                       |                      | Silty Sand & Gravel              |        | Medium dense, brown/gray fine to coarse SAND and Silt, little fine to coarse Gravel    |         |
| 10         | 3               | SS                 | 24   | 20                   | 10.0              | 5          | 2                       | 5      | 6       |                       |                      |                                  |        | Loose, gray fine to coarse SAND, some Silt, trace fine Gravel, (wet)                   |         |
| 15         | 4               | SS                 | 1    | 1                    | 13.5              | 50/1"      |                         |        |         |                       |                      | Bottom of Exploration at 13.6 ft |        | Very dense, gray fine to coarse Gravel   |         |
| 20         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |                                  |        |  |         |
| 25         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |                                  |        |  |         |

Remarks: Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 5 foot screen (0.010 inch slots) and a 10 foot riser. Riser stickup is approximately 2.9 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

- Notes:
- 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.
  - 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.
  - 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer
  - 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BE-4**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT\_12/15/06



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BE-5**  
Page No.: **1 of 1**  
File No.: **0321-005.0**  
Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
Foreman: **Jeff Leavitt**  
GeoDesign Rep.: **Chi Zhang**  
Date Started: **October 9, 2006** Date Finished: **October 10, 2006**  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): **471.0**  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/10/06                 | 12.9       | 458.1      | In well |
| Hammer Fall: | NA                 | 30 in.   | 10/11/06                 | 12.9       | 458.1      | In well |
| Rig Type:    | Bombardier         |          | 10/16/06                 | 12.8       | 458.2      | In well |
| Hammer Type: | Safety - Hydraulic |          | 10/18/06                 | 12.6       | 458.4      | In well |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol               | Sample Description  |                      |                          |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|----------------------|---|----------------------|--------------------------|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |                      |   | Moisture Content (%) | Depth & Elevation (feet) |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |                      |   |                      |                          |
|            | 1               | SS                 | 24   | 10                   | 0.0               | 2          | 3                       | 4      | 7       |         |                       | 1.0                | Topsoil              | Loose, brown SILT, some fine to coarse Sand, trace Roots  |                      |                          |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 2.0                | Subsoil 470.0        |   |                      |                          |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    | Sand & Gravel 469.0  | Dense, brown fine to coarse SAND and fine to coarse GRAVEL, trace Silt                                |                      |                          |
| 5          | 2               | SS                 | 24   | 18                   | 5.0               | 10         | 13                      | 22     | 25      |         |                       |                    |                      |   |                      |                          |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |                      |   |                      |                          |
| 10         | 3               | SS                 | 24   | 24                   | 10.0              | 6          | 7                       | 12     | 12      |         |                       |                    |                      | Medium dense, brown fine to coarse SAND, little fine to coarse Gravel, trace Silt                     |                      |                          |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |                      | Very dense, gray to black fine to coarse GRAVEL and fine to coarse SAND, trace Silt, (weathered Rock) |                      |                          |
| 15         | 4               | SS                 | 24   | 20                   | 15.0              | 16         | 21                      | 37     | 53      |         |                       |                    |                      |   |                      |                          |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |                      |   |                      |                          |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 16.8               | Weathered Rock 454.2 | Bottom of Exploration at 17.5 ft  |                      |                          |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 17.5               | Rock 453.5           |   |                      |                          |
| 20         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |                      |   |                      |                          |
| 25         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |                      |   |                      |                          |

Remarks: Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 10 foot screen (0.010 inch slots) and a 10 foot riser. Riser stickup is approximately 2.6 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BE-5**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name

Stateline Retail Center  
Southeast, New York

Boring No.: **BE-6**  
Page No.: **1 of 1**  
File No.: **0321-005.0**  
Checked By: **ULF**

Boring Company: New England Boring Contractors  
Foreman: Jeff Leavitt  
GeoDesign Rep.: Chi Zhang  
Date Started: October 9, 2009 Date Finished: October 9, 2006  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): 473.0  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/10/06                 | 8.3        | 464.7      | In well |
| Hammer Fall: | NA                 | 30 in.   | 10/11/06                 | 8.3        | 464.7      | In well |
| Rig Type:    | Bombardier         |          | 10/16/06                 | 8.3        | 464.8      | In well |
| Hammer Type: | Safety - Hydraulic |          |                          |            |            |         |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol                           | Sample Description |   |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|----------------------------------|--------------------|---|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |                                  |                    | Moisture Content (%)  |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |                                  |                    |   |
| 0.5        | 1               | SS                 | 24   | 20                   | 0.0               | 4          | 4                       | 6      | 6       |         |                       | 0.5                | Topsoil Silty Sand & Gravel      | 472.5              | Medium dense, red-brown SILT, some fine to coarse Sand, trace Roots                 |
| 5          | 2               | SS                 | 24   | 18                   | 5.0               | 13         | 10                      | 7      | 11      |         |                       |                    |                                  |                    | Medium dense, gray-brown fine to coarse SAND, some Silt, trace fine Gravel          |
| 10         | 3               | SS                 | 24   | 20                   | 10.0              | 6          | 7                       | 12     | 12      |         |                       |                    |                                  |                    | Medium dense, brown SILT and fine to coarse SAND, some fine to coarse Gravel, (wet) |
| 15         | 4               | SS                 | 24   | 20                   | 15.0              | 4          | 4                       | 5      | 7       |         |                       |                    |                                  |                    | Loose, brown fine to coarse SAND, little Silt                                       |
| 20         | 5               | SS                 | 24   | 20                   | 20.0              | 7          | 9                       | 9      | 15      |         |                       |                    |                                  |                    | Medium dense, brown fine to coarse SAND and SILT, trace fine Gravel, (wet)          |
| 22.0       |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 22.0               | Sand & Gravel                    | 451.0              |   |
| 23.5       | 6               | SS                 | 6    | 3                    | 23.0              | 110        |                         |        |         |         |                       | 23.5               | Bottom of Exploration at 23.5 ft | 449.5              | Very dense, brown fine to coarse GRAVEL and fine to coarse SAND, little Silt        |

Remarks: Sample S-4 was lost when box fell from truck. Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 15 foot screen (0.010 inch slots) and a 10 foot riser. Riser stickup is approximately 3.2 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BE-6**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06





**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

# BORING LOG

Project Name

Stateline Retail Center  
Southeast, New York

Boring No.: **BE-7**  
Page No.: 1 of 1  
File No.: 0321-005.0  
Checked By: ULF

Boring Company: New England Boring Contractors  
Foreman: Tim Carpenter  
GeoDesign Rep.: Chi Zhang  
Date Started: October 9, 2006 Date Finished: October 10, 2006  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): 454.0  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |           |
|--------------|--------------------|----------|--------------------------|------------|------------|-----------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes     |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |           |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/9/06                  | 5.0        | 449.0      | Wet spoon |
| Hammer Fall: | NA                 | 30 in.   | 10/10/06                 | 2.2        | 451.8      | In well   |
| Rig Type:    | Bombardier         |          | 10/16/06                 | 2.0        | 452.0      | In well   |
| Hammer Type: | Safety - Hydraulic |          | 10/18/06                 | 1.8        | 452.2      | In well   |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         | Coring Time (min./ft) | Moisture Content (%) | Strata Description | Symbol                           | Sample Description |  |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|-----------------------|----------------------|--------------------|----------------------------------|--------------------|--|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |                       |                      |                    |                                  |                    |  |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 |                       |                      |                    |                                  |                    | 18 - 24  |
|            | 1               | SS                 | 24   | 20                   | 0.0               | 1          | 1                       | 2      | 4       |                       |                      | 1.0                | Topsoil                          |                    | Very loose, dark brown SILT and fine to coarse SAND, little fine to coarse Gravel, trace Roots and Timbers |
| 5          | 2               | SS                 | 24   | 18                   | 5.0               | 8          | 8                       | 12     | 5       |                       |                      | 7.0                | Silty Sand & Gravel              |                    | Medium dense, gray fine to coarse SAND, some fine to coarse Gravel, trace Silt                             |
| 10         | 3               | SS                 | 24   | 20                   | 10.0              | 8          | 9                       | 2      | 2       |                       |                      |                    |                                  |                    | Medium dense, gray fine to coarse SAND, some Silt, some fine to coarse Gravel, (wet)                       |
| 15         | 4               | SS                 | 24   | 12                   | 15.0              | 8          | 8                       | 11     | 11      |                       |                      |                    |                                  |                    | Medium dense, gray SILT and fine to medium SAND  |
| 20         | 5               | SS                 | 24   | 20                   | 20.0              | 20         | 28                      | 33     | 40      |                       |                      | 20.0               | Glacial Till                     |                    | Very dense, gray fine to coarse GRAVEL, some fine to coarse Sand, little Silt                              |
| 25         | 6               | SS                 | 14   | 12                   | 25.0              | 37         | 51                      | 100/2" |         |                       |                      | 26.2               | Bottom of Exploration at 26.2 ft |                    | Very dense, dark gray fine to medium SAND, some Silt, little fine to coarse Gravel                         |

Remarks: Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 15 foot screen (0.010 inch slots) and a 10 foot riser. Riser stickup is approximately 2 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

- Notes:
- 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.
  - 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.
  - 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer
  - 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BE-7**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name

Stateline Retail Center  
Southeast, New York

Boring No.: **BE-8**

Page No.: **1 of 1**

File No.: **0321-005.0**

Checked By: **ULF**

Boring Company: New England Boring Contractors  
Foreman: Tim Carpenter  
GeoDesign Rep.: Chi Zhang  
Date Started: October 6, 2006 Date Finished: October 6, 2006  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): 460.0  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |                          |
|--------------|--------------------|----------|--------------------------|------------|------------|--------------------------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes                    |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |                          |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/6/06                  | 10.0       | 450.0      | Wet sample               |
| Hammer Fall: | NA                 | 30 in.   | 10/6/06                  | 8.0        | 452.0      | Before falling head test |
| Rig Type:    | Bombardier         |          |                          |            |            |                          |
| Hammer Type: | Safety - Hydraulic |          |                          |            |            |                          |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol                           | Sample Description |  |  |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|----------------------------------|--------------------|--|--|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |                                  |                    | Moisture Content (%)   |  |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |                                  |                    |  |  |
| 0.7        | 1               | SS                 | 24   | 10                   | 0.0               | 1          | 2                       | 4      | 4       |         |                       | 0.7                | Topsoil                          |                    | Loose, brow-dark brown fine to coarse SAND and SILT, some fine to coarse Gravel, trace Roots, trace Timber |  |
| 5          | 2               | SS                 | 24   | 20                   | 5.0               | 10         | 13                      | 10     | 9       |         |                       | 459.3              | Sand & Gravel                    |                    |  | Medium dense, brown fine to coarse SAND, little Silt, (moist)                  |
| 10         | 3               | SS                 | 24   | 20                   | 10.0              | 21         | 24                      | 14     | 15      |         |                       | 12.0               | Bottom of Exploration at 12.0 ft |                    |  | Dense, dark brown fine to coarse SAND, some fine to coarse Gravel, little Silt |
| 15         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |                                  |                    |  |  |
| 20         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |                                  |                    |  |  |
| 25         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |                                  |                    |  |  |

Remarks: After taking sample S-3, moved borehole 2 feet to the east and began BE-8A.

Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BE-8**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BE-8A**  
Page No.: **1 of 1**  
File No.: **0321-005.0**  
Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
Foreman: **Tim Carpenter**  
GeoDesign Rep.: **Chi Zhang**  
Date Started: **October 9, 2006** Date Finished: **October 9, 2006**  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): **460.0**  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/10/06                 | 6.9        | 453.1      | In well |
| Hammer Fall: | NA                 | 30 in.   | 10/11/06                 | 6.8        | 453.2      | In well |
| Rig Type:    | Bombardier         |          | 10/16/06                 | 6.7        | 453.3      | In well |
| Hammer Type: | Safety - Hydraulic |          |                          |            |            |         |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         | Coring Time (min./ft) | Moisture Content (%) | Strata Description<br>Depth & Elevation(feet) | Symbol | Sample Description<br>Classification System: Burmister                            |         |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|-----------------------|----------------------|---|--------|---|---------|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |                       |                      |   |        |   |         |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 |                       |                      |   |        |   | 18 - 24 |
| 5          |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |   |        |   |         |
| 10         | 1               | SS                 | 24   | 8                    | 10.0              | 14         | 52                      |        |         |                       |                      | 11.5<br>Boulder                               | 448.5  | Very dense, dark gray fine to coarse SAND, trace Silt                             |         |
| 15         | 2               | SS                 | 24   | 12                   | 15.0              | 15         | 21                      | 29     | 32      |                       |                      | 13.0<br>Glacial Till                          | 447.0  | Very dense, gray-brown fine to coarse SAND and SILT, little fine to coarse Gravel |         |
| 20         | 3               | SS                 | 4    | 4                    | 20.0              | 100/4"     |                         |        |         |                       |                      |   |        | Very dense, gray SILT and fine to coarse SAND, some fine to coarse Gravel         |         |
| 25         | 4               | SS                 | 3    | 3                    | 25.0              | 100/3"     |                         |        |         |                       |                      | 25.3<br>Bottom of Exploration at 25.3 ft      | 434.7  | Very dense, gray SILT, some fine to coarse Sand, some fine to coarse Gravel       |         |

**Remarks:** Boring was located 2 feet east of boring BE-8. (See log B-8 for strata descriptions above 10 foot depth.) Augered to 10 feet below grade for falling head test then began sampling at 10 foot depth; refusal at 11.5 feet; cored boulder to 13 feet. Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 20 foot screen (0.010 inch slots) and a 9 foot riser. Riser stickup is approximately 2.4 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

- Notes:**
- 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.
  - 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.
  - 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer
  - 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BE-8A**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name

Stateline Retail Center  
Southeast, New York

Boring No.: **BW-1**

Page No.: **1 of 2**

File No.: **0321-005.0**

Checked By: **ULF**

Boring Company: New England Boring Contractors  
Foreman: Tim Carpenter  
GeoDesign Rep.: Chi Zhang  
Date Started: October 10, 2006 Date Finished: October 11, 2006  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): 527.0  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/12/06                 | 25.3       | 501.7      | In well |
| Hammer Fall: | NA                 | 30 in.   | 10/12/06                 | 25.5       | 501.5      | In well |
| Rig Type:    | Bombardier         |          | 10/18/06                 | 27.4       | 499.6      | In well |
| Hammer Type: | Safety - Hydraulic |          |                          |            |            |         |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol              | Sample Description |  |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|---------------------|--------------------|--|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |                     |                    | Moisture Content (%)   |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |                     |                    |  |
| 0.5        | 1               | SS                 | 24   | 18                   | 0.0               | 2          | 2                       | 4      | 5       |         |                       | 0.5                | Topsoil Sand & Silt | 526.5              | Loose, brown fine to coarse SAND and SILT, some fine to coarse Gravel, trace Roots |
| 5          | 2               | SS                 | 24   | 20                   | 5.0               | 12         | 12                      | 15     | 15      |         |                       |                    |                     |                    | Medium dense, brown fine to coarse SAND and SILT                                   |
| 10         | 3               | SS                 | 24   | 20                   | 10.0              | 9          | 10                      | 10     | 11      |         |                       |                    |                     |                    | Medium dense, brown fine to coarse SAND and SILT                                   |
| 15         | 4               | SS                 | 24   | 20                   | 15.0              | 10         | 16                      | 27     | 27      |         |                       |                    |                     |                    | Dense, gray SILT and fine to medium SAND   |
| 20         | 5               | SS                 | 24   | 24                   | 20.0              | 25         | 36                      | 40     | 25      |         |                       |                    |                     |                    | Very dense, SILT, some fine to medium SAND   |
| 25         |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 25.0               |                     |                    |  |

Remarks: Hole caved in to 21.5 feet; moist at the bottom. Rollerbit was advanced through weathered rock from 25 to 35 feet below grade. Stopped drilling at 22 feet on 10/10/06 and continued drilling on 10/11/06. Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 15 foot screen (0.010 inch slots) and a 22 foot riser. Riser stickup is approximately 1.1 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BW-1**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

# BORING LOG

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BW-1**  
Page No.: **2 of 2**  
File No.: **0321-005.0**  
Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
Foreman: **Tim Carpenter**  
GeoDesign Rep.: **Chi Zhang**  
Date Started: **October 10, 2006** Date Finished: **October 11, 2006**  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): **527.0**  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/12/06                 | 25.3       | 501.7      | In well |
| Hammer Fall: | NA                 | 30 in.   | 10/12/06                 | 25.5       | 501.5      | In well |
| Rig Type:    | Bombardier         |          | 10/18/06                 | 27.4       | 499.6      | In well |
| Hammer Type: | Safety - Hydraulic |          |                          |            |            |         |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         | Coring Time (min./ft) | Moisture Content (%) | Strata Description | Symbol | Sample Description |         |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|-----------------------|----------------------|--------------------|--------|--------------------|---------|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |                       |                      |                    |        |                    |         |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 |                       |                      |                    |        |                    | 18 - 24 |
|            | 6               | SS                 | 3    | 3                    | 25.0              | 100/3"     |                         |        |         |                       |                      |                    |        |                    |         |
| 30         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |                    |        |                    |         |
| 35         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |                    |        |                    |         |
| 40         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |                    |        |                    |         |
| 45         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |                    |        |                    |         |
| 50         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |                    |        |                    |         |

Remarks

Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BW-1**



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

# BORING LOG

Project Name

Stateline Retail Center  
Southeast, New York

Boring No.: **BW-2**

Page No.: **1 of 2**

File No.: **0321-005.0**

Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
Foreman: **Tim Carpenter**  
GeoDesign Rep.: **Chi Zhang**  
Date Started: **October 12, 2006** Date Finished: **October 12, 2006**  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): **515.0**  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/13/06                 | 25.5       | 489.5      | In well |
| Hammer Fall: | NA                 | 30 in.   |                          |            |            |         |
| Rig Type:    | Bombardier         |          |                          |            |            |         |
| Hammer Type: | Safety - Hydraulic |          |                          |            |            |         |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description             | Symbol | Sample Description   |                      |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------------------|--------|--|----------------------|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                                |        |  | Moisture Content (%) |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                                |        |  |                      |
| 0.5        | 1               | SS                 | 24   | 20                   | 0.0               | 1          | 1                       | 2      | 4       |         |                       | 0.5 Topsoil<br>Glacial<br>Till | 514.5  | Very loose, brown SILT, little fine to coarse Sand, trace Roots                  |                      |
| 5          | 2               | SS                 | 24   | 18                   | 5.0               | 9          | 10                      | 29     | 11      |         |                       |                                |        | Dense, gray fine to coarse SAND and SILT, trace fine to coarse Gravel            |                      |
| 10         | 3               | SS                 | 24   | 20                   | 10.0              | 11         | 23                      | 24     | 36      |         |                       |                                |        | Dense, gray fine to coarse SAND, some Silt, little fine to coarse Gravel         |                      |
| 15         | 4               | SS                 | 16   | 8                    | 15.0              | 51         | 100/4"                  |        |         |         |                       |                                |        | Very dense, gray fine SAND and SILT, trace (-) fine Gravel                       |                      |
| 20         | 5               | SS                 | 15   | 15                   | 20.0              | 41         | 64                      | 101/3" |         |         |                       |                                |        | Very dense, dark gray fine to coarse SAND and SILT, little fine to coarse Gravel |                      |
| 25         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                                |        |  |                      |

**Remarks:** Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 15 foot screen (0.010 inch slots) and a 17 foot riser. Riser stickup is approximately 2.3 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

**Notes:** 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BW-2**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

# BORING LOG

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BW-2**  
Page No.: **2 of 2**  
File No.: **0321-005.0**  
Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
Foreman: **Tim Carpenter**  
GeoDesign Rep.: **Chi Zhang**  
Date Started: **October 12, 2006** Date Finished: **October 12, 2006**  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): **515.0**  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/13/06                 | 25.5       | 489.5      | In well |
| Hammer Fall: | NA                 | 30 in.   |                          |            |            |         |
| Rig Type:    | Bombardier         |          |                          |            |            |         |
| Hammer Type: | Safety - Hydraulic |          |                          |            |            |         |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol | Sample Description |  |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|--------|--------------------|--|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |        |                    | Moisture Content (%)   |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |        |                    |  |
|            | 6               | SS                 | 14   | 12                   | 25.0              | 38         | 60                      | 100/4" |         |         |                       |                    | 26.0   | ▼                  | Classification System: Burmister<br>Very dense, gray fine to medium SAND and SILT, trace fine Gravel |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    | 489.0  |                    |  |
| 30         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    | 30.0   |                    |  |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        | 485.0              |  |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                    | Bottom of Exploration at 30.0 ft   |
| 35         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                    |  |
| 40         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                    |  |
| 45         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                    |  |
| 50         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                    |  |

Remarks

Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BW-2**



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name

Stateline Retail Center  
Southeast, New York

Boring No.: **BW-3**

Page No.: 1 of 1

File No.: 0321-005.0

Checked By: ULF

Boring Company: New England Boring Contractors  
Foreman: Jeff Leavitt  
GeoDesign Rep.: Chi Zhang  
Date Started: October 10, 2006 Date Finished: October 11, 2006  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): 520.0  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/11/06                 | 23.0       | 497.0      | In well |
| Hammer Fall: | NA                 | 30 in.   | 10/11/06                 | 21.3       | 498.7      | In well |
| Rig Type:    | Bombardier         |          | 10/13/06                 | 22.9       | 497.1      | In well |
| Hammer Type: | Safety - Hydraulic |          | 10/18/06                 | 21.9       | 498.1      | In well |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol                           | Sample Description |  |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|----------------------------------|--------------------|--|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |                                  |                    | Moisture Content (%)   |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |                                  |                    |  |
| 0.5        | 1               | SS                 | 24   | 18                   | 0.0               | 9          | 10                      | 13     | 14      |         |                       | 0.5                | Topsoil<br>Glacial<br>Till       | 519.5              | Medium dense, brown SILT and fine to medium SAND, trace Roots                      |
| 5          | 2               | SS                 | 24   | 14                   | 5.0               | 39         | 47                      | 100/5" |         |         |                       |                    |                                  |                    | Very dense, brown fine to medium SAND, some Silt, little fine to coarse Gravel     |
| 10         | 3               | SS                 | 24   | 16                   | 10.0              | 23         | 13                      | 21     | 33      |         |                       |                    |                                  |                    | Dense, gray-light brown SILT and fine to coarse SAND, little fine to coarse Gravel |
| 15         | 4               | SS                 | 11   | 10                   | 15.0              | 67         | 100/5"                  |        |         |         |                       |                    |                                  |                    | Very dense, gray SILT and fine to coarse SAND, trace fine to coarse Gravel         |
| 20         | 5               | SS                 | 3    | 3                    | 20.0              | 100/3"     |                         |        |         |         |                       |                    |                                  |                    | Very dense, brown fine to coarse SAND and fine to coarse GRAVEL                    |
| 25         | 6               | SS                 | 0    | 0                    | 25.0              |            |                         |        |         |         |                       | 25.0               | Bottom of Exploration at 25.0 ft | 495.0              | Refusal  |

Remarks: Spoon refusal at 17 feet below grade. Cored through a 1 foot diameter cobble. Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 10 foot screen (0.010 inch slots) and a 18 foot riser. Riser stickup is approximately 2.6 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

- Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BW-3**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06





**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

# BORING LOG

Project Name

Stateline Retail Center  
Southeast, New York

Boring No.: **BW-4**

Page No.: 1 of 1

File No.: 0321-005.0

Checked By: ULF

Boring Company: New England Boring Contractors  
Foreman: Jeff Leavitt  
GeoDesign Rep.: Chi Zhang  
Date Started: October 11, 2006 Date Finished: October 11, 2006  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): 500.0  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/11/06                 | 14.8       | 485.2      | In well |
| Hammer Fall: | NA                 | 30 in.   | 10/13/06                 | 15.2       | 484.8      | In well |
| Rig Type:    | Bombardier         |          | 10/18/06                 | 15.4       | 484.6      | In well |
| Hammer Type: | Safety - Hydraulic |          |                          |            |            |         |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         | Coring Time (min./ft) | Moisture Content (%) | Strata Description                                | Symbol  | Sample Description |         |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|-----------------------|----------------------|---|---|--------------------|---------|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |                       |                      |   |   |                    |         |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 |                       |                      |   |   |                    | 18 - 24 |
|            | 1               | SS                 | 24   | 8                    | 0.0               | 3          | 3                       | 3      | 4       |                       |                      | Topsoil<br>Silty Sand & Gravel<br>499.6           | Loose, black-gray SILT, some fine to coarse Sand, trace Roots                                 |                    |         |
| 5          | 2               | SS                 | 24   | 16                   | 5.0               | 8          | 13                      | 14     | 14      |                       |                      | 7.5<br>Cobble<br>492.5                            | Medium dense, brown fine to coarse SAND and SILT, trace fine Gravel                           |                    |         |
| 10         | 3               | SS                 | 24   | 14                   | 10.0              | 12         | 15                      | 12     | 14      |                       |                      | 9.0<br>Silty Sand & Gravel<br>491.0               | Medium dense, brown fine to coarse SAND, some Silt, trace fine Gravel                         |                    |         |
| 15         | 4               | SS                 | 24   | 10                   | 15.0              | 12         | 24                      | 24     | 27      |                       |                      | 17.0<br>Decomposed<br>Rock<br>483.0               | Dense, brown fine to coarse SAND, little fine to coarse Gravel, trace Silt, (decomposed Rock) |                    |         |
| 20         | 5               | SS                 | 24   | 22                   | 20.0              | 17         | 26                      | 31     | 39      |                       |                      | 25.0<br>Bottom of Exploration at 25.0 ft<br>475.0 | Very dense, brown/red-brown fine to coarse SAND, little fine to coarse Gravel, trace Silt     |                    |         |

Roller bit was advanced from 22 to 25 feet below grade. Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 10 foot screen (0.010 inch slots) and a 17 foot riser. Riser stickup is approximately 2.5 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

- Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BW-4**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**G E O D E S I G N**  
**I N C O R P O R A T E D**  
 Geotechnical Engineers and Environmental Consultants  
 984 Southford Road  
 Middlebury, Connecticut 06762  
 Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BW-5**  
 Page No.: **1 of 1**  
 File No.: **0321-005.0**  
 Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
 Foreman: **Jeff Leavitt**  
 GeoDesign Rep.: **Chi Zhang**  
 Date Started: **October 11, 2006** Date Finished: **October 12, 2006**  
 N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
 Ground Surface Elevation (feet): **475.0**  
 Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            |          | Sampler: |            | Groundwater Observations |         |  |  |
|--------------|--------------------|----------|----------|------------|--------------------------|---------|--|--|
|              | HW                 | SS       | Date     | Depth (ft) | Elev. (ft)               | Notes   |  |  |
| I.D.:        | 4.0 in.            | 1.38 in. |          |            |                          |         |  |  |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/13/06 | 13.0       | 462.0                    | In well |  |  |
| Hammer Fall: | NA                 | 30 in.   | 10/16/06 | 13.1       | 461.9                    | In well |  |  |
| Rig Type:    | Bombardier         |          | 10/18/06 | 13.1       | 461.9                    | In well |  |  |
| Hammer Type: | Safety - Hydraulic |          |          |            |                          |         |  |  |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol                           | Sample Description  |                      |                          |                                  |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|----------------------------------|---|----------------------|--------------------------|----------------------------------|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |                                  |   | Moisture Content (%) | Depth & Elevation (feet) | Classification System: Burmister |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |                                  |   |                      |                          |                                  |
|            | 1               | SS                 | 13   | 8                    | 0.0               | 3          | 3                       | 100/1" |         |         |                       | 1.0                | Topsoil                          | Very dense, dark brown SILT, little fine to coarse Sand, little fine to coarse Gravel |                      |                          |                                  |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 474.0              | Subsoil & Cobbles                |   |                      |                          |                                  |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 472.5              | Sand & Gravel                    |   |                      |                          |                                  |
| 5          | 2               | SS                 | 24   | 10                   | 5.0               | 7          | 16                      | 13     | 9       |         |                       |                    |                                  | Medium dense, white fine to coarse SAND and fine to coarse GRAVEL                     |                      |                          |                                  |
| 10         | 3               | SS                 | 5    | 3                    | 10.0              | 100/5"     |                         |        |         |         |                       |                    |                                  | Very dense, brown, fine to coarse SAND, little (+) fine GRAVEL, little (-) Silt       |                      |                          |                                  |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 13.0               | Decomposed Bedrock (inferred)    |   |                      |                          |                                  |
| 15         |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 462.0              |                                  |   |                      |                          |                                  |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 458.0              | Bottom of Exploration at 17.0 ft |   |                      |                          |                                  |
| 20         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |                                  |   |                      |                          |                                  |
| 25         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |                                  |   |                      |                          |                                  |

**Remarks**  
 White-colored return water was observed while advancing roller bit from 13 to 17 foot depth. Roller bit refusal at 17 foot depth.  
 Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 10 foot screen (0.010 inch slots) and a 6 foot riser. Riser stickup is approximately 2.3 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

**Notes:**  
 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane;  
 WOR/H = Weight of Rod/Hammer  
 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BW-5**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name

Stateline Retail Center  
Southeast, New York

Boring No.: **BW-6**

Page No.: **1 of 1**

File No.: **0321-005.0**

Checked By: **ULF**

Boring Company: New England Boring Contractors  
Foreman: Jeff Leavitt  
GeoDesign Rep.: Chi Zhang  
Date Started: October 12, 2006 Date Finished: October 13, 2006  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): 486.0  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |           |
|--------------|--------------------|----------|--------------------------|------------|------------|-----------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes     |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |           |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/13/06                 | 11.4       | 474.6      | Open hole |
| Hammer Fall: | NA                 | 30 in.   | 10/16/06                 | 10.5       | 475.5      | In well   |
| Rig Type:    | Bombardier         |          | 10/18/06                 | 10.3       | 475.7      | In well   |
| Hammer Type: | Safety - Hydraulic |          |                          |            |            |           |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol                           | Sample Description |   |                          |   |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|----------------------------------|--------------------|---|--------------------------|---|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |                                  |                    | Moisture Content (%)  | Depth & Elevation (feet) | Classification System: <u>Burmister</u> |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |                                  |                    |   |                          |   |
|            | 1               | SS                 | 24   | 12                   | 0.0               | 1          | 1                       | 2      | 6       |         |                       | 0.5                | Topsoil Sand & Gravel            | 485.5              | Very loose, brown fine SAND, little Silt  |                          |   |
| 5          | 2               | SS                 | 24   | 12                   | 5.0               | 13         | 21                      | 27     | 35      |         |                       |                    |                                  |                    | Dense, brown fine to coarse SAND, some fine to coarse Gravel, trace Silt                              |                          |   |
| 10         | 3               | SS                 | 9    | 6                    | 10.0              | 61         | 100/3"                  |        |         |         |                       | 10.0               | Glacial Till                     | 475.0              | Very dense, black-dark gray SILT and fine to coarse SAND, some fine to coarse Gravel (weathered Rock) |                          |   |
| 15         | 4               | SS                 | 24   | 18                   | 15.0              | 30         | 34                      | 31     | 43      |         |                       |                    |                                  |                    | Very dense, black fine to coarse GRAVEL, some fine to coarse Sand, trace Silt                         |                          |   |
| 20         |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 18.0               | Decomposed Rock (inferred)       | 468.0              |   |                          |   |
| 25         |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 20.0               | Bottom of Exploration at 20.0 ft | 466.0              |   |                          |   |

Remarks: Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 10 foot screen (0.010 inch slots) and a 12 foot riser. Riser stickup is approximately 2.3 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

- Notes:
- 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.
  - 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.
  - 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer
  - 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BW-6**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BW-7**  
Page No.: **1 of 2**  
File No.: **0321-005.0**  
Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
Foreman: **Tim Carpenter**  
GeoDesign Rep.: **Chi Zhang**  
Date Started: **October 10, 2006** Date Finished: **October 11, 2006**  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): **495.0**  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |         |
|--------------|--------------------|----------|--------------------------|------------|------------|---------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes   |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |         |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/12/06                 | 24.5       | 470.5      | In well |
| Hammer Fall: | NA                 | 30 in.   | 10/13/06                 | 24.7       | 470.3      | In well |
| Rig Type:    | Bombardier         |          | 10/15/06                 | 24.7       | 470.3      | In well |
| Hammer Type: | Safety - Hydraulic |          |                          |            |            |         |

| Depth (ft) | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol | Sample Description        |                      |  |   |
|------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|--------|---------------------------|----------------------|--|---|
|            | Casing Blows/ft    |      | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |        |                           | Moisture Content (%) | Depth & Elevation (feet)   | Classification System: <b>Burmister</b> |
|            | Number             | Type |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |        |                           |                      |  |   |
|            | 1                  | SS   | 24                   | 18                | 0.0        | 2                       | 4      | 5       | 7       |                       |                    | 0.5    | Topsoil Sand & Gravel     | 494.5                | Loose, brown SILT, some fine to coarse Sand, trace Roots                             |   |
| 5          | 2                  | SS   | 20                   | 14                | 5.0        | 19                      | 31     | 50      | 50/2"   |                       |                    |        |                           |                      | Very dense, dark brown fine to coarse GRAVEL and fine to coarse SAND, trace Silt     |   |
| 10         | 3                  | SS   | 3                    | 2                 | 10.0       | 100/3"                  |        |         |         |                       |                    |        |                           |                      | Very dense, dark brown SILT, little fine to coarse Sand                              |   |
| 15         |                    |      |                      |                   |            |                         |        |         |         |                       |                    | 13.5   | Decomposed Weathered Rock | 481.5                |  |   |
| 20         | C-1                | C    | 60                   | 60                | 20.0       | [REC= 100%; RQD= 14%]   |        |         |         |                       |                    | 20.0   | Bedrock                   | 475.0                | Very Poor Quality, Soft, Extremely Weathered, dark gray, GNEISS, very close jointing |   |
| 25         |                    |      |                      |                   |            |                         |        |         |         |                       |                    |        |                           |                      |  |   |

Remarks  
Lost water at 19 feet below grade in inferred decomposed rock. Spoon refusal at 13.5 feet below grade; rollerbit advanced to 20 feet. Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 20 foot screen (0.010 inch slots) and a 10 foot riser. Riser stickup is approximately 1.95 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

- Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BW-7**

BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT\_12/15/06



**G E O D E S I G N**  
 I N C O R P O R A T E D  
 Geotechnical Engineers and Environmental Consultants  
 984 Southford Road  
 Middlebury, Connecticut 06762  
 Telephone: 203-758-8836 Fax: 203-758-8842

### BORING LOG

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BW-7**  
 Page No.: **2 of 2**  
 File No.: **0321-005.0**  
 Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
 Foreman: **Tim Carpenter**  
 GeoDesign Rep.: **Chi Zhang**  
 Date Started: **October 10, 2006** Date Finished: **October 11, 2006**  
 N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
 Ground Surface Elevation (feet): **495.0**  
 Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:                   |                 | Sampler:        |             | Groundwater Observations |                |  |  |
|--------------|---------------------------|-----------------|-----------------|-------------|--------------------------|----------------|--|--|
|              | Date                      | Depth (ft)      | Elev. (ft)      | Notes       |                          |                |  |  |
| I.D.:        | <b>4.0 in.</b>            | <b>1.38 in.</b> |                 |             |                          |                |  |  |
| Hammer Wt.:  | <b>NA</b>                 | <b>140 lbs</b>  | <b>10/12/06</b> | <b>24.5</b> | <b>470.5</b>             | <b>In well</b> |  |  |
| Hammer Fall: | <b>NA</b>                 | <b>30 in.</b>   | <b>10/13/06</b> | <b>24.7</b> | <b>470.3</b>             | <b>In well</b> |  |  |
| Rig Type:    | <b>Bombardier</b>         |                 | <b>10/15/06</b> | <b>24.7</b> | <b>470.3</b>             | <b>In well</b> |  |  |
| Hammer Type: | <b>Safety - Hydraulic</b> |                 |                 |             |                          |                |  |  |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         | Coring Time (min./ft) | Moisture Content (%) | Strata Description   | Symbol | Sample Description  |         |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|-----------------------|----------------------|--|--------|---|---------|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |                       |                      |  |        |   |         |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 |                       |                      |  |        |   | 18 - 24 |
|            |                 | C-2                | C    | 42                   | 42                | 25.0       | [REC= 100%; RQD= 30%]   |        |         |                       |                      |  |        | Classification System: <b>Burmister</b><br><br><b>Poor Quality, Moderately Weathered, dark gray, GNEISS, close jointing</b> |         |
|            |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |  |        |   |         |
| 28.5       |                 |                    |      |                      |                   |            |                         |        |         |                       |                      | <b>Bedrock (Continued)</b><br><br><b>28.5</b><br><br><b>Bottom of Exploration at 28.5 ft</b> |        |   |         |
| 30         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |  |        |   |         |
| 35         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |  |        |   |         |
| 40         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |  |        |   |         |
| 45         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |  |        |   |         |
| 50         |                 |                    |      |                      |                   |            |                         |        |         |                       |                      |  |        |   |         |

Remarks

Notes: 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.  
 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.  
 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer  
 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BW-7**



**GEODESIGN**  
INCORPORATED  
Geotechnical Engineers and Environmental Consultants  
984 Southford Road  
Middlebury, Connecticut 06762  
Telephone: 203-758-8836 Fax: 203-758-8842

**BORING LOG**

Project Name  
**Stateline Retail Center**  
**Southeast, New York**

Boring No.: **BW-8**  
Page No.: **1 of 1**  
File No.: **0321-005.0**  
Checked By: **ULF**

Boring Company: **New England Boring Contractors**  
Foreman: **Tim Carpenter**  
GeoDesign Rep.: **Chi Zhang**  
Date Started: **October 12, 2006** Date Finished: **October 13, 2006**  
N. Coordinate: \_\_\_\_\_ E. Coordinate: \_\_\_\_\_  
Ground Surface Elevation (feet): **462.0**  
Station: \_\_\_\_\_ Offset: \_\_\_\_\_ ft

| Type:        | Casing:            | Sampler: | Groundwater Observations |            |            |       |
|--------------|--------------------|----------|--------------------------|------------|------------|-------|
|              | HW                 | SS       | Date                     | Depth (ft) | Elev. (ft) | Notes |
| I.D.:        | 4.0 in.            | 1.38 in. |                          |            |            |       |
| Hammer Wt.:  | NA                 | 140 lbs  | 10/13/06                 | 5.6        | 456.4      |       |
| Hammer Fall: | NA                 | 30 in.   |                          |            |            |       |
| Rig Type:    | Bombardier         |          |                          |            |            |       |
| Hammer Type: | Safety - Hydraulic |          |                          |            |            |       |

| Depth (ft) | Casing Blows/ft | Sample Information |      |                      |                   |            |                         |        |         |         |                       | Strata Description | Symbol       | Sample Description  |                      |
|------------|-----------------|--------------------|------|----------------------|-------------------|------------|-------------------------|--------|---------|---------|-----------------------|--------------------|--------------|---|----------------------|
|            |                 | Number             | Type | Penetration (inches) | Recovery (inches) | Depth (ft) | Blows / 6 inch Interval |        |         |         | Coring Time (min./ft) |                    |              |   | Moisture Content (%) |
|            |                 |                    |      |                      |                   |            | 0 - 6                   | 6 - 12 | 12 - 18 | 18 - 24 |                       |                    |              |   |                      |
|            | 1               | SS                 | 24   | 14                   | 0.0               | 1          | 1                       | 4      | 5       |         |                       | 0.7                | Topsoil      | Loose, dark brown SILT, some fine Sand, trace Roots                                     |                      |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 461.3              | Subsoil      |   |                      |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       | 2.0                | Glacial Till | Medium dense, gray-brown fine to coarse SAND and SILT, some fine to coarse Gravel       |                      |
| 5          | 2               | SS                 | 24   | 20                   | 5.0               | 8          | 11                      | 11     | 8       |         |                       |                    |              |   |                      |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |              | Medium dense, gra-brown fine to coarse GRAVEL and fine to coarse SAND, some Silt, (wet) |                      |
| 10         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |              |   |                      |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |              | Decomposed Rock   |                      |
| 15         | 3               | SS                 | 24   | 20                   | 15.0              | 8          | 10                      | 15     | 15      |         |                       |                    |              |   |                      |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |              | Bottom of Exploration at 25.0 ft  |                      |
| 20         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |              |   |                      |
|            |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |              |   |                      |
| 25         |                 |                    |      |                      |                   |            |                         |        |         |         |                       |                    |              |   |                      |

Remarks: Upon completion of drilling, a 2 inch diameter PVC well was installed. Well consists of a 20 foot screen (0.010 inch slots) and a 7 foot riser. Riser stickup is approximately 2.3 feet. Screen was backfilled with #2 WG filter sand. From 2 feet above screen to 1.5 feet below ground surface well was backfilled with bentonite chips. Locking protective standpipe was concreted in place to protect well.

- Notes:
- 1) Stratification lines represent approximate boundary between material types, transitions may be gradual.
  - 2) Water level readings have been made at times and under conditions stated, fluctuations of groundwater may occur due to other factors than those present at the time measurements were made. AC = After coring; NR = Not Recorded.
  - 3) Abbreviations: A = Auger; C = Core; D = Driven; G = Grab; PS = Piston Sample; SS = Split Spoon; SSL = 3.5 Inch ID Split Spoon; ST = Shelby Tube; V = Vane; WOR/H = Weight of Rod/Hammer
  - 4) Proportions Used: Trace = 1-10%; Little = 10-20%; Some = 20-35%; And = 35-50%

Boring No.: **BW-8**

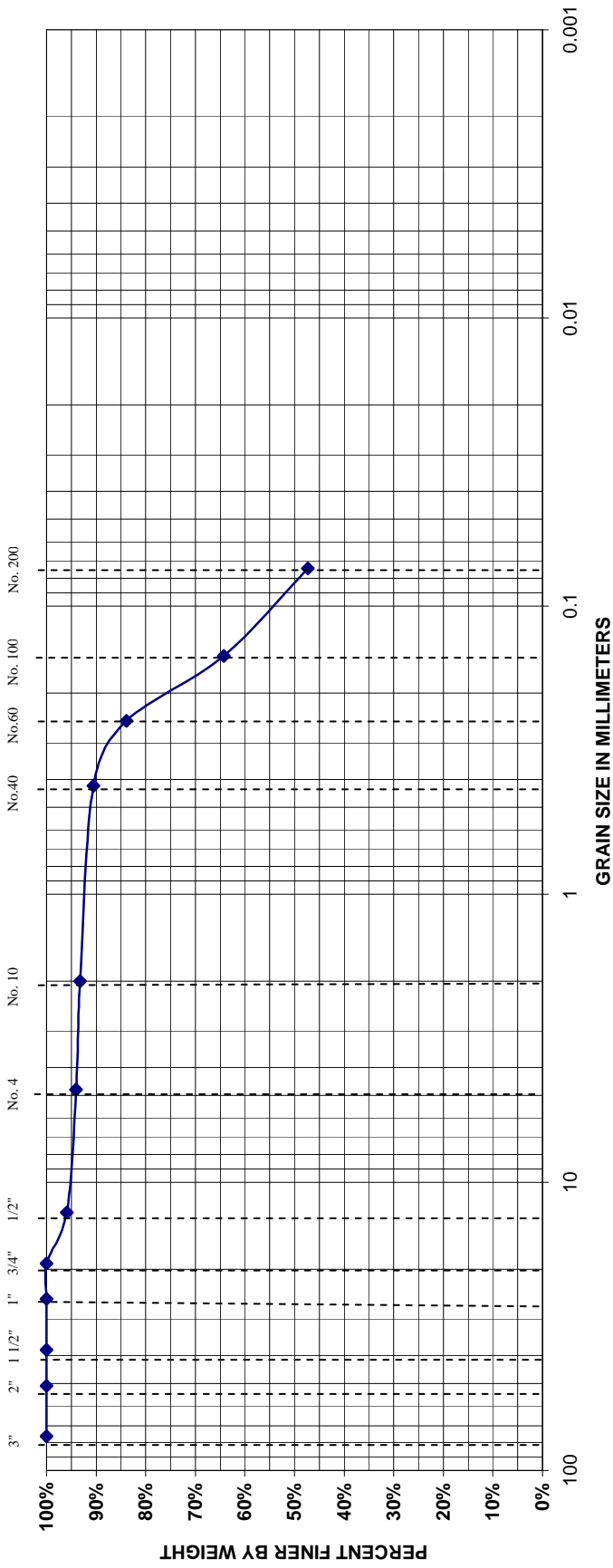
BORING LOG MC 12/19/03 BORING LOGS.GPJ GEODESIGN STANDARD\_GDT 12/15/06

**GRADATION TEST RESULTS**





### U.S. STANDARD SIEVE SIZE



|         |        |        |        |              |
|---------|--------|--------|--------|--------------|
| COBBLES | GRAVEL | SAND   |        | SILT OR CLAY |
|         | FINE   | COARSE | MEDIUM | FINE         |

### GRADATION TEST

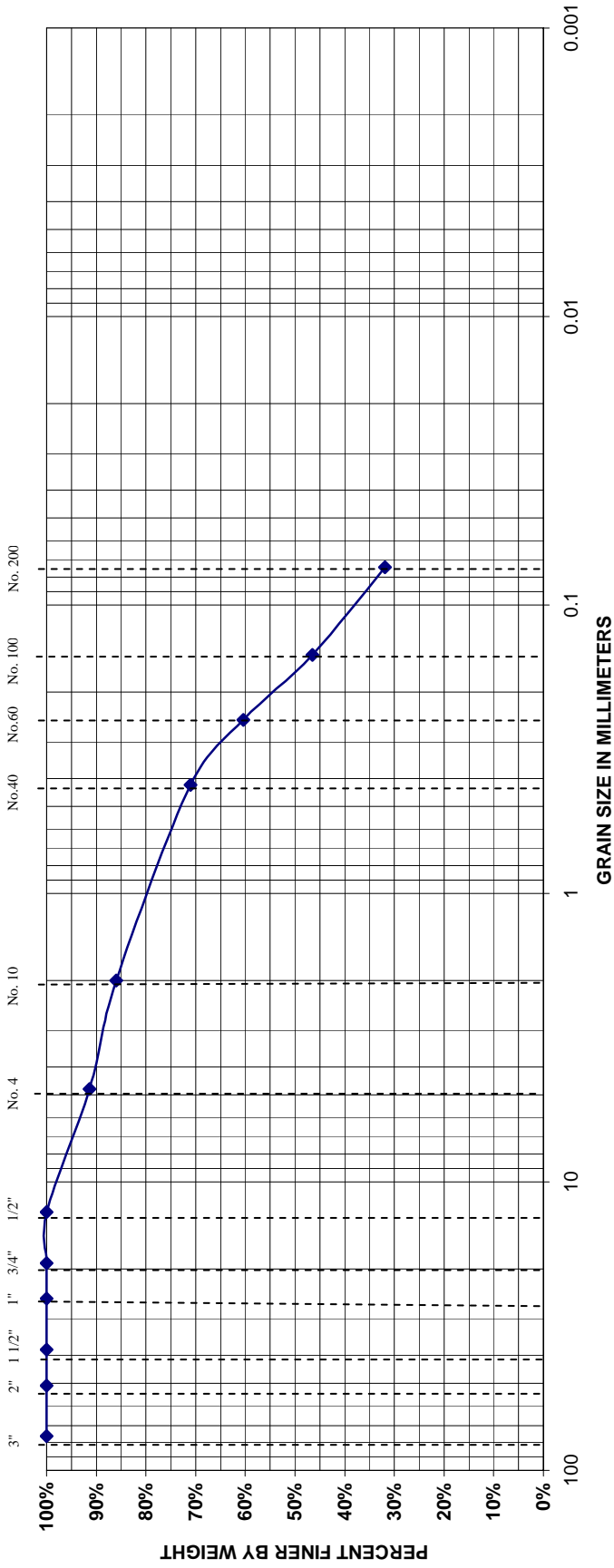
|                       |              |
|-----------------------|--------------|
| Stalene Retail Center |              |
| BORING NO.            | BW 2         |
| SAMPLE NO.            | S-6          |
| DEPTH                 | 2.5' - 2.54" |
| TECH.                 | PAK          |
| REVIEWER              | ULF          |
| DATE                  | 10/18/06     |
| FILE NO.              | 0321-005.0   |

### BURMISTER SOIL CLASSIFICATION SYSTEM

| TEST NO. | MATERIAL SOURCE    | DESCRIPTION                                     |
|----------|--------------------|---|
| 3 of 6   | Split Spoon Sample | SILT and fine to coarse SAND, trace fine Gravel |

**GeoDesign Inc.**  
 984 Southford Road  
 Middlebury, Connecticut 06762  
 (203) 758 8836 (voice)  
 (203) 758 8842 (fax)  
 www.geodesign.net

# U.S. STANDARD SIEVE SIZE



|         |        |                          |              |
|---------|--------|--------------------------|--------------|
| COBBLES | GRAVEL | SAND                     | SILT OR CLAY |
| COARSE  | FINE   | COARSE<br>MEDIUM<br>FINE |              |

## GRADATION TEST

Stateline Retail Center

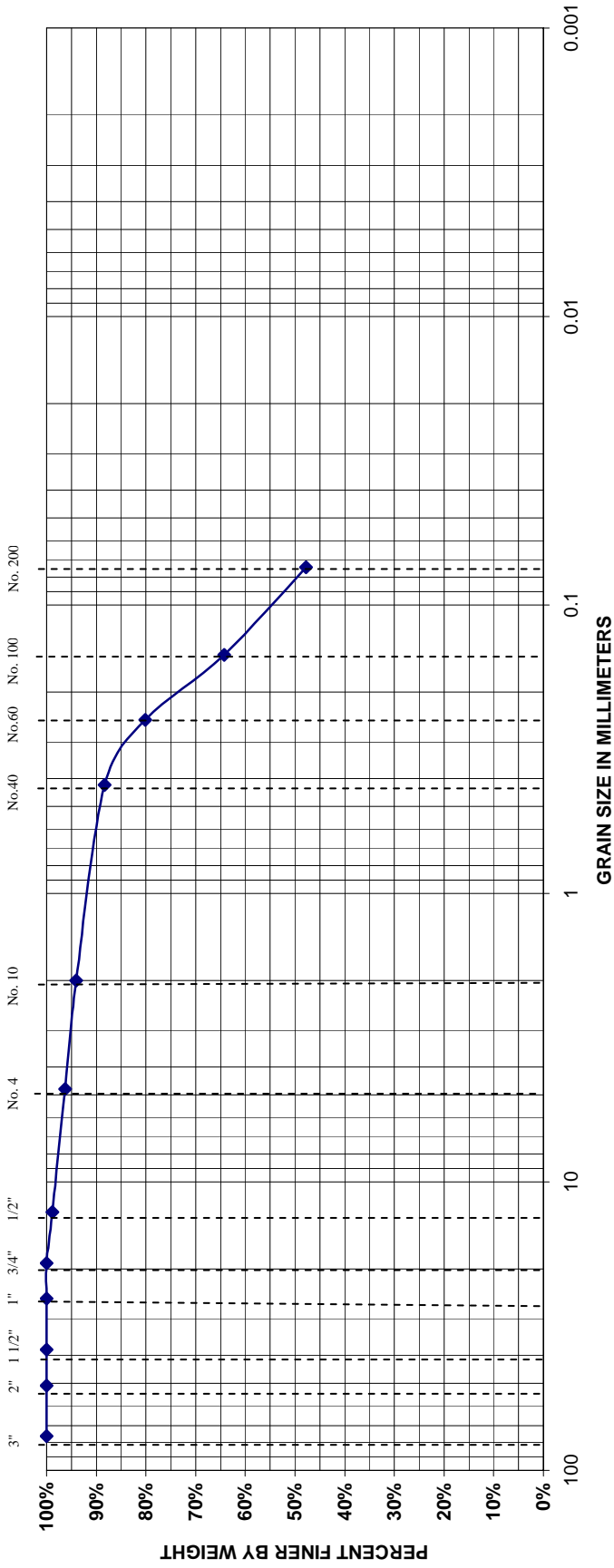
BORING NO. BE 6  
 SAMPLE NO. S-2  
 DEPTH 5'-7"  
 TECH. PAK  
 REVIEWER ULF  
 DATE 10/18/06  
 FILE NO. 0321-005.0

## BURMISTER SOIL CLASSIFICATION SYSTEM

| TEST NO. | MATERIAL SOURCE    | DESCRIPTION  |
|----------|--------------------|--|
| 1 of 6   | Split Spoon Sample | Fine to coarse SAND, some Silt, little fine Gravel |

**GeoDesign Inc.**  
 984 Southford Road  
 Middlebury, Connecticut 06762  
 (203) 758 8836 (voice)  
 (203) 758 8842 (fax)  
 www.geodesign.net

# U.S. STANDARD SIEVE SIZE



|         |        |                          |              |
|---------|--------|--------------------------|--------------|
| COBBLES | GRAVEL | SAND                     | SILT OR CLAY |
| COARSE  | FINE   | COARSE<br>MEDIUM<br>FINE |              |

## GRADATION TEST

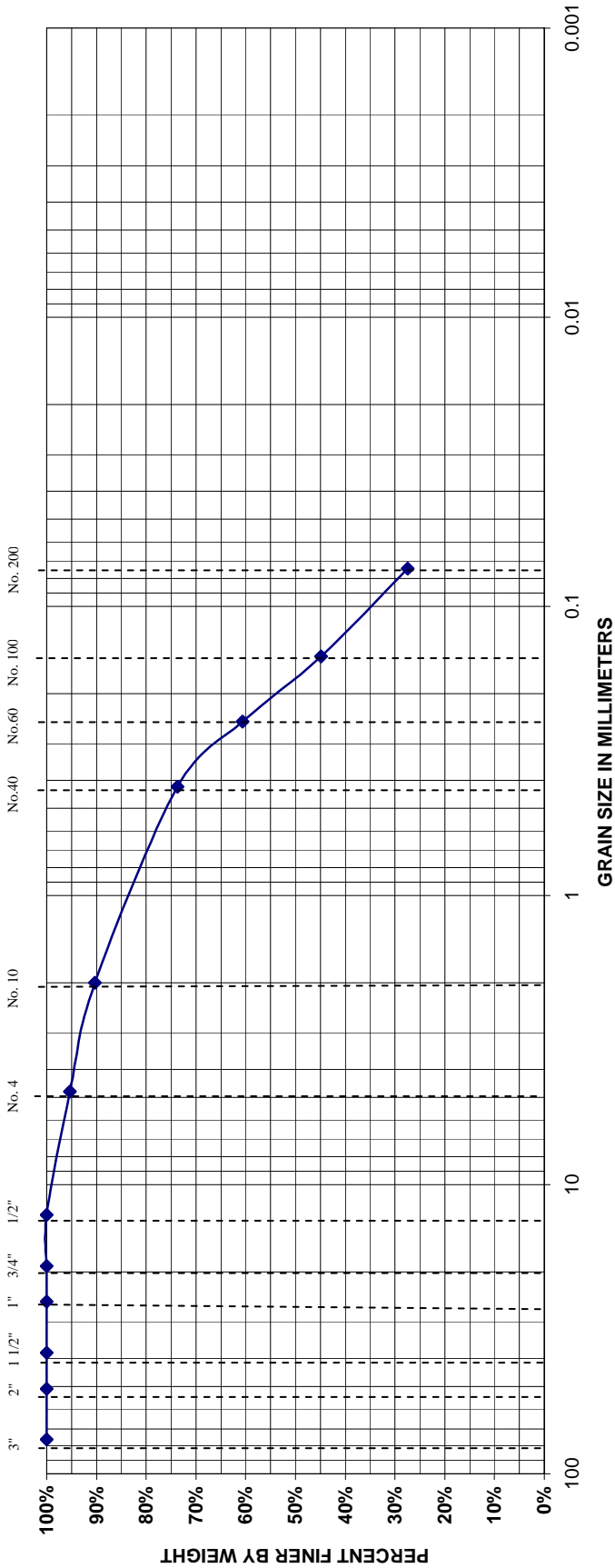
|                       |            |
|-----------------------|------------|
| Stalene Retail Center |            |
| BORING NO.            | BW 2       |
| SAMPLE NO.            | S-4        |
| DEPTH                 | 15'-15'10" |
| TECH.                 | PAK        |
| REVIEWER              | ULF        |
| DATE                  | 10/18/06   |
| FILE NO.              | 0321-005.0 |

## BURMISTER SOIL CLASSIFICATION SYSTEM

| TEST NO. | MATERIAL SOURCE    | DESCRIPTION                                     |
|----------|--------------------|---|
| 5 of 6   | Split Spoon Sample | SILT and fine to coarse Sand, trace fine Gravel |

**GeoDesign Inc.**  
 984 Southford Road  
 Middlebury, Connecticut 06762  
 (203) 758 8836 (voice)  
 (203) 758 8842 (fax)  
 www.geodesign.net

# U.S. STANDARD SIEVE SIZE



|         |        |      |        |      |              |
|---------|--------|------|--------|------|--------------|
| COBBLES | GRAVEL | SAND |        |      | SILT OR CLAY |
|         | COARSE | FINE | COARSE | FINE |              |

## GRADATION TEST

|                         |            |
|-------------------------|------------|
| Stateline Retail Center |            |
| BORING NO.              | BE 4       |
| SAMPLE NO.              | S-3        |
| DEPTH                   | 10'-12'    |
| TECH.                   | PAK        |
| REVIEWER                | ULF        |
| DATE                    | 10/18/06   |
| FILE NO.                | 0321-005.0 |

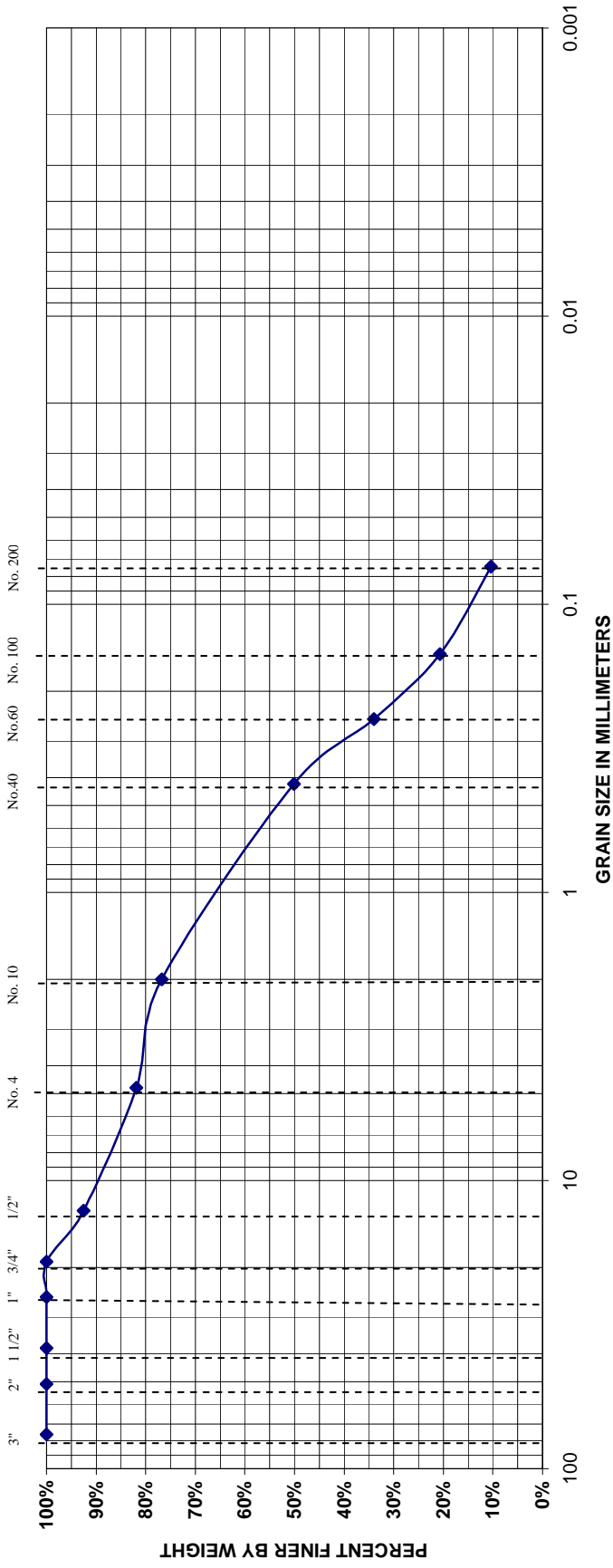
### BURMISTER SOIL CLASSIFICATION SYSTEM

| TEST NO. | MATERIAL SOURCE    | DESCRIPTION                                       |
|----------|--------------------|---|
| 6 of 6   | Split Spoon Sample | Fine to coarse SAND, some Silt, trace fine Gravel |

**GeoDesign Inc.**  
 984 Southford Road  
 Middlebury, Connecticut 06762  
 (203) 758 8836 (voice)  
 (203) 758 8842 (fax)  
 www.geodesign.net



# U.S. STANDARD SIEVE SIZE



|         |        |      |        |        |      |        |              |  |
|---------|--------|------|--------|--------|------|--------|--------------|--|
| COBBLES | GRAVEL |      |        | SAND   |      |        | SILT OR CLAY |  |
|         | COARSE | FINE | COARSE | MEDIUM | FINE | COARSE | FINE         |  |

## GRADATION TEST

|                         |            |
|-------------------------|------------|
| Stateline Retail Center |            |
| BORING NO.              | BW-5       |
| SAMPLE NO.              | S-3        |
| DEPTH                   | 10'-10.5"  |
| TECH.                   | PAK        |
| REVIEWER                | ULF        |
| DATE                    | 10/18/06   |
| FILE NO.                | 0321-005.0 |

### BURMISTER SOIL CLASSIFICATION SYSTEM

| TEST NO. | MATERIAL SOURCE    | DESCRIPTION  |
|----------|--------------------|--|
| 4 of 6   | Split Spoon Sample | Fine to coarse SAND, little (+) fine Gravel, little (-) Silt |

**GeoDesign Inc.**  
 984 Southford Road  
 Middlebury, Connecticut 06762  
 (203) 758 8836 (voice)  
 (203) 758 8842 (fax)  
 www.geodesign.net

IN-SITU FALLING HEAD TEST DATA





Falling Head Test BE-3

| <b>Stateline Retail Center</b><br><b>Southeast, New York</b><br><b>Calculation of Soil Permeability from Falling Head Test Data</b> |                |           |                                     |          |           |                                |                 |                 |
|---|----------------|-----------|-------------------------------------|----------|-----------|--------------------------------|-----------------|-----------------|
| <b>Well No.:</b> BE-3   |                |           | <b>Driller:</b> Tim Carpenter       |          |           | <b>Engineer:</b> Chi Zhang     |                 |                 |
| <b>Test Type:</b> Falling Head  |                |           | <b>Weather:</b> Cloudy, 60's        |          |           |                                |                 |                 |
| <b>Date:</b> 10/6/2006  |                |           |                                     |          |           |                                |                 |                 |
| Ground surface El.: 482.2 (ft.)   |                |           | Depth to Top of Wick: 10.0 (ft.)    |          |           | Length of Wick (L): 2.0 (ft.)  |                 |                 |
| Top of Casing El.: 484.7 (ft.)  |                |           | Depth to Bottom of Wick: 12.0 (ft.) |          |           | Radium of Wick (R): 0.19 (ft.) |                 |                 |
| Top of Wick El.: 472.2 (ft.)  |                |           | Depth to Groundwater: 8.8 (ft.)     |          |           | ln(L/R): 2.36712               |                 |                 |
|   |                |           | Groundwater Elevation: 473.4 (ft.)  |          |           | R^2/2L: 0.10547 (in.)          |                 |                 |
| Elapsed Time (min.)   | t2 - t1 (min.) | DTW (in.) | h1 (in.)                            | h2 (in.) | ln(h1/h2) | k (in/min)                     | k (cm/sec)      | k (ft/day)      |
| 0.00  | 0.00           | 0.0       | 136.1                               |          |           |                                |                 |                 |
| 1.00  | 1.00           | 1.8       | 134.3                               | 134.3    | 0.0133    | <b>3.32E-03</b>                | <b>1.41E-04</b> | <b>3.99E-01</b> |
| 2.00  | 1.00           | 2.1       | 134.0                               | 134.0    | 0.0022    | <b>5.58E-04</b>                | <b>2.36E-05</b> | <b>6.70E-02</b> |
| 4.00  | 2.00           | 3.5       | 132.6                               | 132.6    | 0.0105    | <b>1.31E-03</b>                | <b>5.55E-05</b> | <b>1.57E-01</b> |
| 5.00  | 1.00           | 6.0       | 130.1                               | 130.1    | 0.0190    | <b>4.75E-03</b>                | <b>2.01E-04</b> | <b>5.70E-01</b> |
| 8.00  | 3.00           | 7.0       | 129.1                               | 129.1    | 0.0077    | <b>6.42E-04</b>                | <b>2.72E-05</b> | <b>7.71E-02</b> |
| 10.00   | 2.00           | 9.0       | 127.1                               | 127.1    | 0.0156    | <b>1.95E-03</b>                | <b>8.25E-05</b> | <b>2.34E-01</b> |
| 12.00   | 2.00           | 9.5       | 126.6                               | 126.6    | 0.0039    | <b>4.92E-04</b>                | <b>2.08E-05</b> | <b>5.91E-02</b> |
| 14.00   | 2.00           | 10.5      | 125.6                               | 125.6    | 0.0079    | <b>9.90E-04</b>                | <b>4.19E-05</b> | <b>1.19E-01</b> |
| 16.00   | 2.00           | 11.0      | 125.1                               | 125.1    | 0.0040    | <b>4.98E-04</b>                | <b>2.11E-05</b> | <b>5.98E-02</b> |
| 18.00   | 2.00           | 12.0      | 124.1                               | 124.1    | 0.0080    | <b>1.00E-03</b>                | <b>4.24E-05</b> | <b>1.20E-01</b> |
| 20.00   | 2.00           | 13.0      | 123.1                               | 123.1    | 0.0081    | <b>1.01E-03</b>                | <b>4.28E-05</b> | <b>1.21E-01</b> |
| 22.00   | 2.00           | 14.0      | 122.1                               | 122.1    | 0.0082    | <b>1.02E-03</b>                | <b>4.31E-05</b> | <b>1.22E-01</b> |
| 24.00   | 2.00           | 15.0      | 121.1                               | 121.1    | 0.0082    | <b>1.03E-03</b>                | <b>4.35E-05</b> | <b>1.23E-01</b> |
| 26.00   | 8.00           | 16.0      | 120.1                               | 120.1    | 0.0328    | <b>1.02E-03</b>                | <b>4.33E-05</b> | <b>1.23E-01</b> |
| 30.00   | 4.00           | 17.0      | 119.1                               | 119.1    | 0.0084    | <b>5.22E-04</b>                | <b>2.21E-05</b> | <b>6.26E-02</b> |
| 75.00   | 45.00          | 28.0      | 108.1                               | 108.1    | 0.0969    | <b>5.38E-04</b>                | <b>2.28E-05</b> | <b>6.45E-02</b> |

|                 |                 |                 |                 |
|-----------------|-----------------|-----------------|-----------------|
| Maximun k Value | <b>4.75E-03</b> | <b>2.01E-04</b> | <b>5.70E-01</b> |
| Minimun k Value | <b>4.92E-04</b> | <b>2.08E-05</b> | <b>5.91E-02</b> |
| Average k Value | <b>1.29E-03</b> | <b>5.47E-05</b> | <b>1.55E-01</b> |

- Notes:
1. Ground surface elevations were interpolated from existing contours, and are approximate.
  2. Groundwater levels were measured during drilling.

| <b>Stateline Retail Center</b><br><b>Southeast, New York</b><br><b>Calculation of Soil Permeability from Falling Head Test Data</b> |                |             |                               |          |             |                            |                 |                 |
|---|----------------|-------------|-------------------------------|----------|-------------|----------------------------|-----------------|-----------------|
| <b>Well No.:</b> BE-4   |                |             | <b>Driller:</b> Tim Carpenter |          |             | <b>Engineer:</b> Chi Zhang |                 |                 |
| <b>Test Type:</b> Falling Head  |                |             | <b>Weather:</b> Cloudy, 60's  |          |             |                            |                 |                 |
| <b>Date:</b> 10/6/2006  |                |             |                               |          |             |                            |                 |                 |
| Ground surface El.:   |                | 473.0 (ft.) | Depth to Top of Wick:         |          | 10.0 (ft.)  | Length of Wick (L):        |                 | 2.4 (ft.)       |
| Top of Casing El.:  |                | 476.0 (ft.) | Depth to Bottom of Wick:      |          | 12.0 (ft.)  | Radium of Wick (R):        |                 | 0.20 (ft.)      |
| Top of Wick El.:  |                | 463.0 (ft.) | Depth to Groundwater:         |          | 13.8 (ft.)  | ln(L/R):                   |                 | 2.44925         |
|   |                |             | Groundwater Elevation:        |          | 459.3 (ft.) | R^2/2L:                    |                 | 0.10547 (in.)   |
| Elapsed Time (min.)   | t2 - t1 (min.) | DTW (in.)   | h1 (in.)                      | h2 (in.) | ln(h1/h2)   | k (in/min)                 | k (cm/sec)      | k (ft/day)      |
| 0.75  | 0.00           | 57.6        | 143.5                         |          |             |                            |                 |                 |
| 1.25  | 0.50           | 74.4        | 126.7                         | 126.7    | 0.1245      | <b>6.43E-02</b>            | <b>2.72E-03</b> | <b>7.72E+00</b> |
| 1.75  | 0.50           | 81.6        | 119.5                         | 119.5    | 0.0585      | <b>3.02E-02</b>            | <b>1.28E-03</b> | <b>3.63E+00</b> |
| 2.25  | 0.50           | 87.6        | 113.5                         | 113.5    | 0.0515      | <b>2.66E-02</b>            | <b>1.13E-03</b> | <b>3.19E+00</b> |
| 2.75  | 0.50           | 91.2        | 109.9                         | 109.9    | 0.0322      | <b>1.66E-02</b>            | <b>7.05E-04</b> | <b>2.00E+00</b> |
| 3.25  | 0.50           | 96.0        | 105.1                         | 105.1    | 0.0447      | <b>2.31E-02</b>            | <b>9.77E-04</b> | <b>2.77E+00</b> |
| 3.75  | 0.50           | 99.6        | 101.5                         | 101.5    | 0.0348      | <b>1.80E-02</b>            | <b>7.62E-04</b> | <b>2.16E+00</b> |
| 4.25  | 0.50           | 103.2       | 97.9                          | 97.9     | 0.0361      | <b>1.87E-02</b>            | <b>7.90E-04</b> | <b>2.24E+00</b> |
| 5.25  | 1.00           | 108.0       | 93.1                          | 93.1     | 0.0503      | <b>1.30E-02</b>            | <b>5.50E-04</b> | <b>1.56E+00</b> |
| 6.75  | 1.50           | 112.8       | 88.3                          | 88.3     | 0.0529      | <b>9.11E-03</b>            | <b>3.86E-04</b> | <b>1.09E+00</b> |
| 7.75  | 1.00           | 117.6       | 83.5                          | 83.5     | 0.0559      | <b>1.44E-02</b>            | <b>6.11E-04</b> | <b>1.73E+00</b> |
| 8.75  | 1.00           | 120.0       | 81.1                          | 81.1     | 0.0292      | <b>7.53E-03</b>            | <b>3.19E-04</b> | <b>9.04E-01</b> |
| 15.00   | 6.25           | 129.6       | 71.5                          | 71.5     | 0.1260      | <b>5.21E-03</b>            | <b>2.20E-04</b> | <b>6.25E-01</b> |
| 18.90   | 3.90           | 132.0       | 69.1                          | 69.1     | 0.0341      | <b>2.26E-03</b>            | <b>9.57E-05</b> | <b>2.71E-01</b> |
| 22.83   | 3.93           | 134.4       | 66.7                          | 66.7     | 0.0353      | <b>2.32E-03</b>            | <b>9.83E-05</b> | <b>2.79E-01</b> |
| 27.83   | 5.00           | 136.8       | 64.3                          | 64.3     | 0.0366      | <b>1.89E-03</b>            | <b>8.01E-05</b> | <b>2.27E-01</b> |
| 34.67   | 6.84           | 138.0       | 63.1                          | 63.1     | 0.0188      | <b>7.11E-04</b>            | <b>3.01E-05</b> | <b>8.53E-02</b> |
| 44.50   | 9.83           | 140.4       | 60.7                          | 60.7     | 0.0388      | <b>1.02E-03</b>            | <b>4.31E-05</b> | <b>1.22E-01</b> |
| Maximun k Value   |                |             |                               |          |             | <b>6.43E-02</b>            | <b>2.72E-03</b> | <b>7.72E+00</b> |
| Minimun k Value   |                |             |                               |          |             | <b>3.02E-02</b>            | <b>1.28E-03</b> | <b>3.63E+00</b> |
| Average k Value   |                |             |                               |          |             | <b>2.66E-02</b>            | <b>1.13E-03</b> | <b>3.19E+00</b> |

- Notes:
1. Ground surface elevations were interpolated from existing contours, and are approximate.
  2. Groundwater levels were measured during drilling.
  3. Volume of pea stone used to fill the wick was approximately 139% of the theoretical volume of cavity (casing O.D. x length of wick) Raidus and length of wick were adjusted accordingly using the actual volume of pea stone used.

| <b>Stateline Retail Center</b><br><b>Southeast, New York</b><br><b>Calculation of Soil Permeability from Falling Head Test Data</b> |                |           |                                     |          |           |                                |                 |                 |
|---|----------------|-----------|-------------------------------------|----------|-----------|--------------------------------|-----------------|-----------------|
| <b>Well No.:</b> BE-5   |                |           | <b>Driller:</b> Jeff Leavitt        |          |           |                                |                 |                 |
| <b>Test Type:</b> Falling Head  |                |           | <b>Engineer:</b> Chi Zhang          |          |           |                                |                 |                 |
| <b>Date:</b> 10/9/2006  |                |           | <b>Weather:</b> Cloudy, 60's        |          |           |                                |                 |                 |
| Ground surface El.: 469.0 (ft.)   |                |           | Depth to Top of Wick: 13.0 (ft.)    |          |           | Length of Wick (L): 2.1 (ft.)  |                 |                 |
| Top of Casing El.: 471.6 (ft.)  |                |           | Depth to Bottom of Wick: 15.0 (ft.) |          |           | Radium of Wick (R): 0.19 (ft.) |                 |                 |
| Top of Wick El.: 456.0 (ft.)  |                |           | Depth to Groundwater: 12.9 (ft.)    |          |           | ln(L/R): 2.40131               |                 |                 |
|   |                |           | Groundwater Elevation: 456.1 (ft.)  |          |           | R^2/2L: 0.10547 (in.)          |                 |                 |
| Elapsed Time (min.)   | t2 - t1 (min.) | DTW (in.) | h1 (in.)                            | h2 (in.) | ln(h1/h2) | k (in/min)                     | k (cm/sec)      | k (ft/day)      |
| 0.00  | 0.00           | 0.0       | 186.5                               |          |           |                                |                 |                 |
| 0.50  | 0.50           | 16.8      | 169.7                               | 169.7    | 0.0944    | <b>4.78E-02</b>                | <b>2.02E-03</b> | <b>5.74E+00</b> |
| 1.50  | 1.00           | 25.2      | 161.3                               | 161.3    | 0.0508    | <b>1.29E-02</b>                | <b>5.44E-04</b> | <b>1.54E+00</b> |
| 2.00  | 0.50           | 26.4      | 160.1                               | 160.1    | 0.0075    | <b>3.78E-03</b>                | <b>1.60E-04</b> | <b>4.54E-01</b> |
| 2.50  | 0.50           | 31.2      | 155.3                               | 155.3    | 0.0304    | <b>1.54E-02</b>                | <b>6.53E-04</b> | <b>1.85E+00</b> |
| 3.00  | 0.50           | 33.6      | 152.9                               | 152.9    | 0.0156    | <b>7.89E-03</b>                | <b>3.34E-04</b> | <b>9.47E-01</b> |
| 4.25  | 1.25           | 39.6      | 146.9                               | 146.9    | 0.0400    | <b>8.11E-03</b>                | <b>3.43E-04</b> | <b>9.73E-01</b> |
| 5.75  | 1.50           | 43.2      | 143.3                               | 143.3    | 0.0248    | <b>4.19E-03</b>                | <b>1.77E-04</b> | <b>5.03E-01</b> |
| 7.75  | 2.00           | 58.8      | 127.7                               | 127.7    | 0.1153    | <b>1.46E-02</b>                | <b>6.18E-04</b> | <b>1.75E+00</b> |
| 10.00   | 2.25           | 68.4      | 118.1                               | 118.1    | 0.0782    | <b>8.80E-03</b>                | <b>3.72E-04</b> | <b>1.06E+00</b> |
| 13.00   | 3.00           | 80.4      | 106.1                               | 106.1    | 0.1072    | <b>9.05E-03</b>                | <b>3.83E-04</b> | <b>1.09E+00</b> |
| 15.00   | 2.00           | 88.8      | 97.7                                | 97.7     | 0.0825    | <b>1.04E-02</b>                | <b>4.42E-04</b> | <b>1.25E+00</b> |
| 20.00   | 5.00           | 103.2     | 83.3                                | 83.3     | 0.1595    | <b>8.08E-03</b>                | <b>3.42E-04</b> | <b>9.69E-01</b> |
| 25.00   | 5.00           | 115.2     | 71.3                                | 71.3     | 0.1556    | <b>7.88E-03</b>                | <b>3.34E-04</b> | <b>9.46E-01</b> |
| 30.00   | 5.00           | 126.0     | 60.5                                | 60.5     | 0.1643    | <b>8.32E-03</b>                | <b>3.52E-04</b> | <b>9.99E-01</b> |
| Maximun k Value   |                |           |                                     |          |           | <b>4.78E-02</b>                | <b>2.02E-03</b> | <b>5.74E+00</b> |
| Minimun k Value   |                |           |                                     |          |           | <b>3.78E-03</b>                | <b>1.60E-04</b> | <b>4.54E-01</b> |
| Average k Value   |                |           |                                     |          |           | <b>1.19E-02</b>                | <b>5.06E-04</b> | <b>1.43E+00</b> |

- Notes:
1. Ground surface elevations were interpolated from existing contours, and are approximate.
  2. Groundwater levels were measured during drilling.
  3. Volume of pea stone used to fill the wick was approximately 115% of the theoretical volume of cavity (casing O.D. x length of wick). Radius and length of wick were adjusted accordingly using the actual volume of pea stone used.

Falling Head Test BE-8

| <b>Stateline Retail Center</b><br><b>Southeast, New York</b><br><b>Calculation of Soil Permeability from Falling Head Test Data</b> |                |           |                                     |          |           |                                |                 |                 |
|---|----------------|-----------|-------------------------------------|----------|-----------|--------------------------------|-----------------|-----------------|
| <b>Well No.:</b> BE-8   |                |           | <b>Driller:</b> Tim Carpenter       |          |           | <b>Engineer:</b> Chi Zhang     |                 |                 |
| <b>Test Type:</b> Falling Head  |                |           | <b>Weather:</b> Sunny, 70's         |          |           |                                |                 |                 |
| <b>Date:</b> 10/9/2006  |                |           |                                     |          |           |                                |                 |                 |
| Ground surface El.: 460.8 (ft.)   |                |           | Depth to Top of Wick: 10.5 (ft.)    |          |           | Length of Wick (L): 2.1 (ft.)  |                 |                 |
| Top of Casing El.: 463.3 (ft.)  |                |           | Depth to Bottom of Wick: 12.5 (ft.) |          |           | Radium of Wick (R): 0.19 (ft.) |                 |                 |
| Top of Wick El.: 450.3 (ft.)  |                |           | Depth to Groundwater: 8.0 (ft.)     |          |           | ln(L/R): 2.38816               |                 |                 |
|   |                |           | Groundwater Elevation: 452.8 (ft.)  |          |           | R^2/2L: 0.10547 (in.)          |                 |                 |
| Elapsed Time (min.)   | t2 - t1 (min.) | DTW (in.) | h1 (in.)                            | h2 (in.) | ln(h1/h2) | k (in/min)                     | k (cm/sec)      | k (ft/day)      |
| 0.00  | 0.00           | 0.0       | 125.5                               |          |           |                                |                 |                 |
| 0.50  | 0.50           | 5.0       | 120.5                               | 120.5    | 0.0406    | <b>2.05E-02</b>                | <b>8.67E-04</b> | <b>2.46E+00</b> |
| 1.50  | 1.00           | 13.0      | 112.5                               | 112.5    | 0.0687    | <b>1.73E-02</b>                | <b>7.32E-04</b> | <b>2.08E+00</b> |
| 2.00  | 0.50           | 16.0      | 109.5                               | 109.5    | 0.0270    | <b>1.36E-02</b>                | <b>5.76E-04</b> | <b>1.63E+00</b> |
| 2.50  | 0.50           | 18.0      | 107.5                               | 107.5    | 0.0184    | <b>9.28E-03</b>                | <b>3.93E-04</b> | <b>1.11E+00</b> |
| 3.00  | 0.50           | 21.0      | 104.5                               | 104.5    | 0.0283    | <b>1.43E-02</b>                | <b>6.03E-04</b> | <b>1.71E+00</b> |
| 4.25  | 1.25           | 26.0      | 99.5                                | 99.5     | 0.0490    | <b>9.88E-03</b>                | <b>4.18E-04</b> | <b>1.19E+00</b> |
| 5.75  | 1.50           | 31.0      | 94.5                                | 94.5     | 0.0515    | <b>8.66E-03</b>                | <b>3.66E-04</b> | <b>1.04E+00</b> |
| 7.75  | 2.00           | 38.0      | 87.5                                | 87.5     | 0.0769    | <b>9.69E-03</b>                | <b>4.10E-04</b> | <b>1.16E+00</b> |
| 10.00   | 2.25           | 44.0      | 81.5                                | 81.5     | 0.0710    | <b>7.95E-03</b>                | <b>3.37E-04</b> | <b>9.54E-01</b> |
| 13.00   | 3.00           | 52.0      | 73.5                                | 73.5     | 0.1033    | <b>8.67E-03</b>                | <b>3.67E-04</b> | <b>1.04E+00</b> |
| 14.00   | 1.00           | 55.0      | 70.5                                | 70.5     | 0.0417    | <b>1.05E-02</b>                | <b>4.44E-04</b> | <b>1.26E+00</b> |
| 15.00   | 1.00           | 57.0      | 68.5                                | 68.5     | 0.0288    | <b>7.25E-03</b>                | <b>3.07E-04</b> | <b>8.70E-01</b> |
| 24.00   | 9.00           | 73.0      | 52.5                                | 52.5     | 0.2659    | <b>7.44E-03</b>                | <b>3.15E-04</b> | <b>8.93E-01</b> |
| 30.00   | 6.00           | 82.0      | 43.5                                | 43.5     | 0.1880    | <b>7.89E-03</b>                | <b>3.34E-04</b> | <b>9.47E-01</b> |
| 43.00   | 13.00          | 91.0      | 34.5                                | 34.5     | 0.2317    | <b>4.49E-03</b>                | <b>1.90E-04</b> | <b>5.39E-01</b> |
| 53.00   | 10.00          | 98.0      | 27.5                                | 27.5     | 0.2266    | <b>5.71E-03</b>                | <b>2.42E-04</b> | <b>6.85E-01</b> |
| 63.00   | 10.00          | 102.0     | 23.5                                | 23.5     | 0.1571    | <b>3.96E-03</b>                | <b>1.67E-04</b> | <b>4.75E-01</b> |

|                 |                 |                 |                 |
|-----------------|-----------------|-----------------|-----------------|
| Maximun k Value | <b>2.05E-02</b> | <b>8.67E-04</b> | <b>2.46E+00</b> |
| Minimun k Value | <b>3.96E-03</b> | <b>1.67E-04</b> | <b>4.75E-01</b> |
| Average k Value | <b>9.82E-03</b> | <b>4.16E-04</b> | <b>1.18E+00</b> |

- Notes:
1. Ground surface elevations were interpolated from existing contours, and are approximate.
  2. Groundwater levels were measured during drilling.
  3. Volume of pea stone used to fill the wick was approximately 109% of the theoretical volume of cavity (casing O.D. x length of wick) Raidus and length of wick were adjusted accordingly using the actual volume of pea stone used.

Falling Head Test BW-6

| <b>Stateline Retail Center</b><br><b>Southeast, New York</b><br><b>Calculation of Soil Permeability from Falling Head Test Data</b> |                |           |                                     |          |           |                                |            |            |
|---|----------------|-----------|-------------------------------------|----------|-----------|--------------------------------|------------|------------|
| <b>Well No.:</b> BW-6   |                |           | <b>Driller:</b> Tim Carpenter       |          |           | <b>Engineer:</b> Chi Zhang     |            |            |
| <b>Test Type:</b> Falling Head  |                |           | <b>Weather:</b> Sunny, 60's         |          |           |                                |            |            |
| <b>Date:</b> 10/13/2006   |                |           |                                     |          |           |                                |            |            |
| Ground surface El.: 486.0 (ft.)   |                |           | Depth to Top of Wick: 15.0 (ft.)    |          |           | Length of Wick (L): 2.0 (ft.)  |            |            |
| Top of Casing El.: 488.1 (ft.)  |                |           | Depth to Bottom of Wick: 17.0 (ft.) |          |           | Radium of Wick (R): 0.19 (ft.) |            |            |
| Top of Wick El.: 471.0 (ft.)  |                |           | Depth to Groundwater: 11.4 (ft.)    |          |           | ln(L/R): 2.36712               |            |            |
|   |                |           | Groundwater Elevation: 474.6 (ft.)  |          |           | R^2/2L: 0.10547 (in.)          |            |            |
| Elapsed Time (min.)   | t2 - t1 (min.) | DTW (in.) | h1 (in.)                            | h2 (in.) | ln(h1/h2) | k (in/min)                     | k (cm/sec) | k (ft/day) |
| 0.00  | 0.00           | 0.0       | 162.4                               |          |           |                                |            |            |
| 1.50  | 1.50           | 0.3       | 162.1                               | 162.1    | 0.0015    | 2.56E-04                       | 1.09E-05   | 3.08E-02   |
| 2.50  | 1.00           | 0.8       | 161.6                               | 161.6    | 0.0031    | 7.71E-04                       | 3.26E-05   | 9.25E-02   |
| 3.50  | 1.00           | 1.0       | 161.4                               | 161.4    | 0.0015    | 3.87E-04                       | 1.64E-05   | 4.64E-02   |
| 4.25  | 0.75           | 1.3       | 161.1                               | 161.1    | 0.0016    | 5.16E-04                       | 2.18E-05   | 6.19E-02   |
| 5.00  | 0.75           | 1.5       | 160.9                               | 160.9    | 0.0016    | 5.17E-04                       | 2.19E-05   | 6.20E-02   |
| 5.83  | 0.83           | 1.8       | 160.6                               | 160.6    | 0.0016    | 4.66E-04                       | 1.97E-05   | 5.59E-02   |
| 6.33  | 0.50           | 2.0       | 160.4                               | 160.4    | 0.0016    | 7.83E-04                       | 3.31E-05   | 9.40E-02   |
| 7.00  | 0.67           | 2.3       | 160.1                               | 160.1    | 0.0016    | 5.81E-04                       | 2.46E-05   | 6.98E-02   |
| 7.83  | 0.83           | 2.5       | 159.9                               | 159.9    | 0.0016    | 4.68E-04                       | 1.98E-05   | 5.62E-02   |
| 8.50  | 0.67           | 2.8       | 159.6                               | 159.6    | 0.0016    | 5.86E-04                       | 2.48E-05   | 7.03E-02   |
| 9.00  | 0.50           | 3.0       | 159.4                               | 159.4    | 0.0016    | 7.83E-04                       | 3.31E-05   | 9.39E-02   |
| 10.50   | 1.50           | 3.5       | 158.9                               | 158.9    | 0.0031    | 5.23E-04                       | 2.21E-05   | 6.28E-02   |
| 11.83   | 1.33           | 4.0       | 158.4                               | 158.4    | 0.0032    | 5.92E-04                       | 2.51E-05   | 7.10E-02   |
| 13.00   | 1.17           | 4.5       | 157.9                               | 157.9    | 0.0032    | 6.75E-04                       | 2.86E-05   | 8.10E-02   |
| 14.67   | 1.67           | 5.0       | 157.4                               | 157.4    | 0.0032    | 4.74E-04                       | 2.01E-05   | 5.69E-02   |
| 17.58   | 2.91           | 6.0       | 156.4                               | 156.4    | 0.0064    | 5.46E-04                       | 2.31E-05   | 6.56E-02   |
| 20.75   | 3.17           | 7.0       | 155.4                               | 155.4    | 0.0064    | 5.06E-04                       | 2.14E-05   | 6.07E-02   |
| 24.00   | 3.25           | 8.0       | 154.4                               | 154.4    | 0.0065    | 4.96E-04                       | 2.10E-05   | 5.95E-02   |
| 27.25   | 3.25           | 9.0       | 153.4                               | 153.4    | 0.0065    | 4.99E-04                       | 2.11E-05   | 5.99E-02   |
| 31.17   | 3.92           | 10.0      | 152.4                               | 152.4    | 0.0065    | 4.17E-04                       | 1.77E-05   | 5.00E-02   |

|                 |          |          |          |
|-----------------|----------|----------|----------|
| Maximun k Value | 7.83E-04 | 3.31E-05 | 9.40E-02 |
| Minimun k Value | 3.87E-04 | 1.64E-05 | 4.64E-02 |
| Average k Value | 5.45E-04 | 2.31E-05 | 6.54E-02 |

- Notes:
1. Ground surface elevations were interpolated from existing contours, and are approximate.
  2. Groundwater levels were measured during drilling.

| <b>Stateline Retail Center</b><br><b>Southeast, New York</b><br><b>Calculation of Soil Permeability from Falling Head Test Data</b> |                |           |                                     |          |           |                                |            |            |          |
|---|----------------|-----------|-------------------------------------|----------|-----------|--------------------------------|------------|------------|----------|
| <b>Well No.:</b> BW-8   |                |           | <b>Driller:</b> Tim Carpenter       |          |           |                                |            |            |          |
| <b>Test Type:</b> Falling Head  |                |           | <b>Engineer:</b> Chi Zhang          |          |           |                                |            |            |          |
| <b>Date:</b> 10/13/2006   |                |           | <b>Weather:</b> Sunny, 60's         |          |           |                                |            |            |          |
| Ground surface El.: 462.9 (ft.)   |                |           | Depth to Top of Wick: 15.0 (ft.)    |          |           | Length of Wick (L): 2.0 (ft.)  |            |            |          |
| Top of Casing El.: 465.2 (ft.)  |                |           | Depth to Bottom of Wick: 17.0 (ft.) |          |           | Radium of Wick (R): 0.19 (ft.) |            |            |          |
| Top of Wick El.: 447.9 (ft.)  |                |           | Depth to Groundwater: 11.4 (ft.)    |          |           | ln(L/R): 2.36712               |            |            |          |
|   |                |           | Groundwater Elevation: 451.5 (ft.)  |          |           | R^2/2L: 0.10547 (in.)          |            |            |          |
| Elapsed Time (min.)   | t2 - t1 (min.) | DTW (in.) | h1 (in.)                            | h2 (in.) | ln(h1/h2) | k (in/min)                     | k (cm/sec) | k (ft/day) |          |
| 0.00  | 0.00           | 29.0      | 135.5                               |          |           |                                |            |            |          |
| 1.00  | 1.00           | 30.0      | 134.5                               | 134.5    | 0.0074    | 1.85E-03                       | 7.83E-05   | 2.22E-01   |          |
| 1.50  | 0.50           | 34.0      | 130.5                               | 130.5    | 0.0302    | 1.51E-02                       | 6.38E-04   | 1.81E+00   |          |
| 2.00  | 0.50           | 36.0      | 128.5                               | 128.5    | 0.0154    | 7.71E-03                       | 3.26E-04   | 9.25E-01   |          |
| 2.50  | 0.50           | 38.0      | 126.5                               | 126.5    | 0.0157    | 7.83E-03                       | 3.32E-04   | 9.40E-01   |          |
| 3.50  | 1.00           | 41.0      | 123.5                               | 123.5    | 0.0240    | 5.99E-03                       | 2.54E-04   | 7.19E-01   |          |
| 4.00  | 0.50           | 43.0      | 121.5                               | 121.5    | 0.0163    | 8.15E-03                       | 3.45E-04   | 9.78E-01   |          |
| 4.50  | 0.50           | 44.0      | 120.5                               | 120.5    | 0.0083    | 4.13E-03                       | 1.75E-04   | 4.95E-01   |          |
| 5.00  | 0.50           | 46.0      | 118.5                               | 118.5    | 0.0167    | 8.36E-03                       | 3.54E-04   | 1.00E+00   |          |
| 6.00  | 1.00           | 48.0      | 116.5                               | 116.5    | 0.0170    | 4.25E-03                       | 1.80E-04   | 5.10E-01   |          |
| 7.00  | 1.00           | 49.0      | 115.5                               | 115.5    | 0.0086    | 2.15E-03                       | 9.11E-05   | 2.58E-01   |          |
| 8.00  | 1.00           | 51.0      | 113.5                               | 113.5    | 0.0175    | 4.36E-03                       | 1.85E-04   | 5.23E-01   |          |
| 9.00  | 1.00           | 52.5      | 112.0                               | 112.0    | 0.0133    | 3.32E-03                       | 1.41E-04   | 3.99E-01   |          |
| 11.00   | 2.00           | 55.5      | 109.0                               | 109.0    | 0.0271    | 3.39E-03                       | 1.43E-04   | 4.07E-01   |          |
| 13.00   | 2.00           | 58.0      | 106.5                               | 106.5    | 0.0232    | 2.90E-03                       | 1.23E-04   | 3.48E-01   |          |
| 15.00   | 10.00          | 60.0      | 104.5                               | 104.5    | 0.1257    | 3.14E-03                       | 1.33E-04   | 3.77E-01   |          |
| 17.00   | 2.00           | 62.0      | 102.5                               | 102.5    | 0.0193    | 2.41E-03                       | 1.02E-04   | 2.89E-01   |          |
| 19.00   | 2.00           | 64.0      | 100.5                               | 100.5    | 0.0197    | 2.46E-03                       | 1.04E-04   | 2.95E-01   |          |
| 23.00   | 4.00           | 68.0      | 96.5                                | 96.5     | 0.0406    | 2.53E-03                       | 1.07E-04   | 3.04E-01   |          |
| 27.00   | 4.00           | 71.0      | 93.5                                | 93.5     | 0.0316    | 1.97E-03                       | 8.34E-05   | 2.36E-01   |          |
| 30.00   | 3.00           | 73.0      | 91.5                                | 91.5     | 0.0216    | 1.80E-03                       | 7.62E-05   | 2.16E-01   |          |
| 37.00   | 7.00           | 76.0      | 88.5                                | 88.5     | 0.0333    | 1.19E-03                       | 5.03E-05   | 1.43E-01   |          |
| 41.00   | 4.00           | 78.0      | 86.5                                | 86.5     | 0.0229    | 1.43E-03                       | 6.04E-05   | 1.71E-01   |          |
|   |                |           |                                     |          |           | Maximun k Value                | 1.51E-02   | 6.38E-04   | 1.81E+00 |
|   |                |           |                                     |          |           | Minimun k Value                | 1.19E-03   | 5.03E-05   | 1.43E-01 |
|   |                |           |                                     |          |           | Average k Value                | 3.97E-03   | 1.68E-04   | 4.77E-01 |

- Notes:
1. Ground surface elevations were interpolated from existing contours, and are approximate.
  2. Groundwater levels were measured during drilling.

## TABLES





Table No. 1

Groundwater and Well Data

Stateline Retail Center  
Southeast, NY

| Well No. | Ref. Elev. | G.S. Elev. | Stickup | Well Depth Below GS | 10/9/2006 |     | 10/10/2006 |      | 10/11/2006 |       | 10/12/2006 |      | 10/13/2006 |      | 10/16/2006 |       | 10/19/2006 |     | October Data Only |     |     |       |            |            |                           |               |  |  |  |
|----------|------------|------------|---------|---------------------|-----------|-----|------------|------|------------|-------|------------|------|------------|------|------------|-------|------------|-----|-------------------|-----|-----|-------|------------|------------|---------------------------|---------------|--|--|--|
|          |            |            |         |                     | DBR       | DTW | Elev.      | DBR  | DTW        | Elev. | DBR        | DTW  | Elev.      | DBR  | DTW        | Elev. | DBR        | DTW | Elev.             | DBR | DTW | Elev. | Min. Elev. | Mean Elev. | Range between Min and Max | DTW from mean |  |  |  |
| BE-1     | 488.1      | 484.9      | 3.2     | 18.5                | 9.1       | 5.8 | 479.1      | 10.4 | 7.1        | 477.8 |            |      |            |      |            |       |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BE-2     | 493.4      | 490.9      | 2.5     | 31.0                |           |     |            | 12.9 | 10.4       | 480.5 | 12.8       | 10.3 | 480.6      |      |            |       |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BE-3     | 484.7      | 482.2      | 2.5     | 12.0                |           |     |            | 11.0 | 8.5        | 473.7 | 11.1       | 8.6  | 473.6      |      |            |       |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BE-4     | 476.0      | 473.0      | 3.0     | 13.6                |           |     |            | 12.0 | 9.0        | 464.0 |            |      |            |      |            |       |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BE-5     | 471.6      | 469.0      | 2.6     | 17.5                |           |     |            | 15.5 | 12.8       | 456.2 | 15.5       | 12.8 | 456.2      |      |            |       |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BE-6     | 472.1      | 468.8      | 3.3     | 23.5                |           |     |            | 11.5 | 8.2        | 460.6 | 11.5       | 8.2  | 460.6      |      |            |       |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BE-7     | 456.6      | 454.6      | 2.0     | 26.2                |           |     |            | 4.2  | 2.2        | 452.4 | 4.2        | 2.2  | 452.4      |      |            |       |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BE-8     | 463.3      | 460.8      | 2.5     | 25.0                |           |     |            | 9.3  | 6.9        | 453.9 | 9.2        | 6.7  | 454.1      |      |            |       |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BW-1     | 532.1      | 529.9      | 2.2     | 25.0                |           |     |            |      |            |       | 26.4       | 24.2 | 505.7      |      |            |       |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BW-2     | 519.4      | 517.1      | 2.3     | 30.0                |           |     |            |      |            |       |            |      |            | 27.8 | 25.4       | 491.7 |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BW-3     | 522.3      | 519.5      | 2.8     | 25.0                |           |     |            | 23.9 | 21.2       | 498.3 |            |      |            | 25.5 | 22.8       | 496.7 |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BW-4     | 501.2      | 498.6      | 2.6     | 25.0                |           |     |            | 17.3 | 14.7       | 483.9 |            |      |            | 17.7 | 15.1       | 483.5 |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BW-5     | 478.3      | 475.9      | 2.4     | 25.0                |           |     |            |      |            |       |            |      |            | 15.2 | 12.9       | 463.1 |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BW-6     | 488.1      | 486.0      | 2.1     | 20.0                |           |     |            |      |            |       |            |      |            | 15.3 | 13.0       | 463.0 |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BW-7     | 499.5      | 497.4      | 2.1     | 28.5                |           |     |            |      |            |       | 26.6       | 24.6 | 472.8      | 12.8 | 10.7       | 475.3 |            |     |                   |     |     |       |            |            |                           |               |  |  |  |
| BW-8     | 465.21     | 462.90     | 2.31    | 25.0                |           |     |            |      |            |       | 26.4       | 24.4 | 473.0      | 7.8  | 5.5        | 457.4 |            |     |                   |     |     |       |            |            |                           |               |  |  |  |

Notes:

- 1) Ref Elev. = Reference Elevation marked on top of solid PVC well riser inside protective casing.
- 2) DTW = Depth to Water Below Ground Surface
- 3) GS = Ground Surface
- 4) Elev. = Groundwater Surface Elevation
- 5) DBR = Depth below reference
- 6) All data is stated in feet.
- 7) Well locations located by GeoDesign by taping from existing site features. Well elevations surveyed by Insite Engineering.

**TABLE No. 2**  
**Summary of Depth to Bedrock**

**Stateline Retail Center**  
**Southeast, NY**

**East SSDS Area**

| Boring | Ground Surface Elevation (ft.) | Depth to Top of Bedrock (ft.) | Bedrock Elevation (ft.) | RQD 0-5' run (%) | RQD 5'-10' run (%) | Notes   |
|--------|--------------------------------|-------------------------------|-------------------------|------------------|--------------------|---|
| BE-1A  | 484.0                          | 8.5                           | 475.5                   | 100              | 90                 |   |
| BE-2   | 490.0                          | 21.0                          | 469.0                   | 90               | 70                 | A layer of cobbles and boulders exists from Elev.479 to Elev. 469 |
| BE-3   | 483.0                          | 7.0                           | 476.0                   | N/A              | N/A                | Weathered Rock inferred from spoon sample and roller bit          |
| BE-4   | 473.0                          | N/A                           | N/A                     | N/A              | N/A                | Spoon Refusal at Elev. 459.4                                      |
| BE-5   | 471.0                          | 10.8                          | 460.2                   | N/A              | N/A                | Weathered Rock inferred from spoon sample and roller bit          |
| BE-6   | 473.0                          | N/A                           | N/A                     | N/A              | N/A                | Spoon Refusal at Elev. 449.5                                      |
| BE-7   | 454.0                          | N/A                           | N/A                     | N/A              | N/A                | Spoon Refusal at Elev. 427.8                                      |
| BE-8A  | 460.0                          | N/A                           | N/A                     | N/A              | N/A                | Spoon Refusal at Elev. 434.7                                      |

**West SSDS Area**

| Boring | Ground Surface Elevation (ft.) | Depth to Top of Bedrock (ft.) | Bedrock Elevation (ft.) | RQD 0-5' run (%) | RQD 5'-10' run (%) | Notes  |
|--------|--------------------------------|-------------------------------|-------------------------|------------------|--------------------|--|
| BW-1   | 0.00                           | 20                            | -20.00                  | N/A              | N/A                | Roller bit 10 feet through the weathered rock to refusal, did not core |
| BW-2   | 0.00                           | 26                            | -26.00                  | N/A              | N/A                | Roller bit 5 feet through the weathered rock to refusal, did not core  |
| BW-3   | 0.00                           | N/A                           | N/A                     | N/A              | N/A                | Spoon Refusal: infer bedrock   |
| BW-4   | 0.00                           | 17                            | -17.00                  | N/A              | N/A                | Roller bit 8 feet through the weathered rock to refusal, did not core  |
| BW-5   | 0.00                           | 13                            | -13.00                  | N/A              | N/A                | Roller bit 4 feet through the weathered rock to refusal, did not core  |
| BW-6   | 0.00                           | 18                            | -18.00                  | N/A              | N/A                | Roller bit 2 feet through the weathered rock to refusal, did not core  |
| BW-7   | 0.00                           | 13.5                          | -13.50                  | 14.4             | 50                 | Roller bit 6.5 into decomposed rock and core 10 feet                   |
| BW-8   | 0.00                           | 19                            | -19.00                  | N/A              | N/A                | Roller bit 5 feet through the weathered rock to refusal, did not core  |

Note: 1. RQD = Rock Quality Designation. Defined as the total length of sound core pieces, 4 inches or greater in length, expressed as a percentage of the total length cored.

**Table No. 3**  
**Summary of Average Soil Permeability**

**Stateline Retail Center**  
**Southeast, New York**

| <b>Falling Head Test Data</b> |                 |                     |                 |                 |
|-------------------------------|-----------------|---------------------|-----------------|-----------------|
| <b>Area</b>                   | <b>Well No.</b> | <b>Permeability</b> |                 |                 |
|                               |                 | <b>(in/sec)</b>     | <b>(cm/sec)</b> | <b>(ft/day)</b> |
| <b>East Area</b>              | BE-3            | 1.29E-03            | 5.47E-05        | 1.55E-01        |
|                               | BE-4            | 2.66E-02            | 1.13E-03        | 3.19E+00        |
|                               | BE-5            | 1.19E-02            | 5.06E-04        | 1.43E+00        |
|                               | BE-8            | 9.82E-03            | 4.16E-04        | 1.18E+00        |
|                               | <b>Average</b>  | <b>1.24E-02</b>     | <b>5.26E-04</b> | <b>1.49E+00</b> |
| <b>West Area</b>              | BW-6            | 5.45E-04            | 2.31E-05        | 6.54E-02        |
|                               | BW-8            | 3.97E-03            | 1.68E-04        | 4.77E-01        |
|                               | <b>Average</b>  | <b>2.26E-03</b>     | <b>9.56E-05</b> | <b>2.71E-01</b> |

**Table No. 4**  
**Kozeny - Carman Analyses**  
**to Estimate Coefficient of Permeability**

**Stateline Retail Center**  
**Southeast, New York**

| Area      | Test Boring No. | Sample No. | Sample Depth (ft.)      | D <sub>10</sub> (mm) | SPT "N"-value (blows / ft) | Descriptive Density | Relative Density (%) | in-situ void ratio e | in-situ porosity n | Coefficient of Permeability k (cm/sec) | Coefficient of Permeability k (ft/day) |
|-----------|-----------------|------------|-------------------------|----------------------|----------------------------|---------------------|----------------------|----------------------|--------------------|--|--|
| West Area | BW-2            | S-4        | 15'-15' <sup>10</sup> " | 0.007                | 100                        | Very dense          | 100                  | 0.140                | 0.12               | 5.54E-07                               | 1.57E-03                               |
|           | BW-2            | S-6        | 25'-25' <sup>4</sup> "  | 0.007                | 160                        | Very dense          | 100                  | 0.140                | 0.12               | 5.54E-07                               | 1.57E-03                               |
|           | BW-5            | S-3        | 10'-10' <sup>5</sup> "  | 0.075                | 100                        | Very dense          | 100                  | 0.140                | 0.12               | 6.36E-05                               | 1.80E-01                               |
| East Area | BE-4            | S-2        | 5'-7'                   | 0.075                | 23                         | Medium Dense        | 50                   | 0.495                | 0.33               | 2.14E-03                               | 6.08E+00                               |
|           | BE-4            | S-3        | 10'-12'                 | 0.015                | 7                          | Loose               | 25                   | 0.673                | 0.40               | 1.92E-04                               | 5.45E-01                               |
|           | BE-6            | S-2        | 5'-7'                   | 0.003                | 17                         | Medium Dense        | 45                   | 0.531                | 0.35               | 4.13E-06                               | 1.17E-02                               |

| SPT (bl/ft) | Descriptive Density | Relative Density (%) |
|-------------|---------------------|----------------------|
| 0 to 4      | Very loose          | 0 to 15              |
| 4 to 10     | Loose               | 15 to 35             |
| 10 to 30    | Medium Dense        | 35 to 65             |
| 30 to 50    | Dense               | 65 to 85             |
| 50 +        | Very dense          | 85 to 100            |

| emin | emax |
|------|------|
| 0.14 | 0.85 |

**West Area** Minimum: 5.54E-07  
Maximum: 6.36E-05  
**Average: 2.16.E-05**

**East Area** Minimum: 4.13E-06  
Maximum: 2.14E-03  
**Average: 7.80.E-04**

**References:**

- 1.) Lambe & Whitman p 30 and p 287 and Kozeny-Carman Method

**Table No. 5  
Effluent Flow Analysis**

**Stateline Retail Center  
Southeast, New York**

| effluent flow gal/day | input source flow (ft <sup>3</sup> /d)            | East Area<br>Input over 8 50-ft long cells<br>(north-south direction)<br>No. of cells = 8<br>Q total | West Area<br>Input over 4 50-ft long cells<br>(north-south direction)<br>No. of cells = 4<br>Q total |
|-----------------------|---|--|--|
| 500                   | 66.8  | 4,000 gpd  | 2,000 gpd  |
| 625                   | 83.6  | 5,000 gpd  | 2,500 gpd  |
| 750                   | 100.3   | 6,000 gpd  | 3,000 gpd  |
| 875                   | 117.0   | 7,000 gpd  | 3,500 gpd  |
| 1000                  | 133.7   | 8,000 gpd  | 4,000 gpd  |
| 1250                  | 167.1   | 10,000 gpd   | 5,000 gpd  |
| 1500                  | 200.5   | 12,000 gpd   | 6,000 gpd  |
| 2000                  | 267.4   | 16,000 gpd   | 8,000 gpd  |
| 3000                  | 401.1   | 24,000 gpd   | 12,000 gpd   |
|                       | Avg. Width of Recharge Area (East West Direction) | 400 feet   | 800 feet   |

Flow into model (at cell 10)

from Darcy  $Q=ka$ , max flow into model is about 2.8 ft<sup>3</sup>/day per foot  
 2.8                      450                      1260 ft<sup>3</sup>/day  
 say 1000 ft<sup>3</sup>/day  
 also no rainfall flow

Adjustment to Transmissivity resulting from increased saturated flow thickness

|                                   | East Area | West Area        |
|-----------------------------------|-----------|------------------|
| Existing Site Avg. Depth to Water | 8 ft      | 17               |
| Existing Site Avg. Sat Thickness  | 13.6 ft   | 8                |
| Max gw rise (8' - 3' = 5')        | 5         | (17' - 3' = 14') |
| Proposed Max Sat Thickness        | 18.6      | 22               |
| ratio                             | 1.37      | 2.75             |
| Say                               | 1.3       | 2                |

Table No. 6A

Historical Precipitation at Station KPOU  
Poughkeepsie, NY

| Precip.<br>(in) | Month |      |      |      |      |      |       |      |      |      |      |      | TOTAL |
|-----------------|-------|------|------|------|------|------|-------|------|------|------|------|------|-------|
|                 | J     | F    | M    | A    | M    | J    | J     | A    | S    | O    | N    | D    |       |
| 1835            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1836            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1837            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1838            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1839            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1840            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1841            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1842            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1843            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1844            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1845            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1846            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1847            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1848            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1849            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1850            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1851            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1852            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1853            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1854            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1855            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1856            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1857            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1858            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1859            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1860            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1861            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1862            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1863            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1864            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1865            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1866            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1867            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1868            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1869            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1870            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1871            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1872            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1873            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1874            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1875            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1876            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1877            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1878            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1879            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1880            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1881            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1882            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1883            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1884            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1885            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1886            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1887            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1888            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1889            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1890            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1891            | -     | -    | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1892            | -     | 1.00 | 2.30 | -    | -    | -    | 5.86  | -    | -    | -    | -    | -    | -     |
| 1893            | 2.17  | 6.24 | -    | -    | -    | -    | -     | -    | -    | -    | -    | -    | -     |
| 1894            | -     | -    | -    | -    | -    | -    | -     | 1.37 | -    | -    | -    | -    | -     |
| 1895            | -     | -    | -    | -    | -    | -    | -     | -    | 1.16 | 3.45 | 3.70 | 3.03 | -     |
| 1896            | 1.05  | 5.49 | 6.12 | 0.87 | 3.28 | 3.57 | 3.96  | 2.92 | 4.30 | 2.31 | 2.98 | 1.37 | 38.22 |
| 1897            | 2.11  | 2.22 | 2.74 | 2.41 | 5.42 | 2.77 | 15.71 | 3.75 | 1.62 | 1.06 | 4.46 | 4.39 | 48.66 |
| 1898            | 3.54  | 3.46 | 2.23 | 3.35 | 6.38 | 0.95 | 3.87  | 8.77 | 3.35 | 5.08 | 3.16 | 2.68 | 46.82 |
| 1899            | 2.70  | 4.00 | 5.32 | 1.69 | 1.75 | 4.57 | 5.84  | 0.86 | 6.51 | 1.26 | 1.78 | 1.79 | 38.07 |
| 1900            | 2.82  | 5.33 | 3.36 | 1.81 | 4.20 | 2.17 | 4.28  | 3.14 | 2.78 | 2.80 | 3.86 | 2.07 | 38.62 |
| 1901            | 1.57  | 0.70 | 4.88 | 8.26 | 6.43 | 1.23 | 6.47  | 7.20 | 3.59 | 2.28 | 1.66 | 6.16 | 50.43 |

Table No. 6A

Historical Precipitation at Station KPOU  
Poughkeepsie, NY

| Precip.<br>(in) | Month |      |      |      |      |       |       |       |      |       |      |      | TOTAL |
|-----------------|-------|------|------|------|------|-------|-------|-------|------|-------|------|------|-------|
|                 | J     | F    | M    | A    | M    | J     | J     | A     | S    | O     | N    | D    |       |
| 1902            | 2.38  | 4.13 | 4.12 | 3.28 | 2.33 | 4.55  | 7.57  | 2.34  | 6.21 | 5.56  | 0.99 | 5.37 | 48.83 |
| 1903            | 3.09  | 4.40 | 3.88 | 2.61 | 0.74 | 10.90 | 3.26  | 7.96  | 2.29 | 6.17  | 1.53 | 2.73 | 49.56 |
| 1904            | 2.51  | 2.35 | 2.91 | 3.34 | 2.29 | 2.65  | 4.48  | 6.00  | 4.20 | 2.74  | 1.34 | 1.84 | 36.65 |
| 1905            | 3.27  | 1.35 | 2.75 | 2.28 | 0.79 | 4.10  | 4.30  | 4.46  | 4.79 | 2.16  | 1.74 | 2.73 | 34.72 |
| 1906            | 2.56  | 2.05 | 3.72 | 4.82 | 3.71 | 2.84  | 6.36  | 3.10  | 2.26 | 3.56  | 1.43 | 4.21 | 40.62 |
| 1907            | 3.19  | 2.39 | 2.08 | 2.15 | 3.50 | 3.42  | 2.53  | 2.04  | 6.11 | 4.95  | 4.35 | 4.39 | 41.10 |
| 1908            | 2.38  | 5.13 | 2.15 | 2.11 | 5.93 | 1.43  | 4.48  | 3.81  | 0.78 | 1.99  | 0.63 | 2.43 | 33.25 |
| 1909            | 3.00  | 4.79 | 2.66 | 5.41 | 2.25 | 2.15  | 2.96  | 5.46  | 3.60 | 0.90  | 1.31 | 3.66 | 38.15 |
| 1910            | 4.93  | 2.86 | 1.03 | 4.77 | 2.77 | 4.38  | 2.10  | 4.11  | 2.04 | 1.39  | 3.43 | 2.05 | 35.86 |
| 1911            | 2.20  | 2.61 | 2.99 | 2.80 | 1.88 | 5.43  | 2.82  | 6.46  | 2.44 | 5.67  | 2.67 | 3.01 | 40.98 |
| 1912            | 1.24  | 1.91 | 5.87 | 3.55 | 3.72 | 1.54  | 3.00  | 3.66  | 2.96 | 2.86  | 2.25 | 4.12 | 36.68 |
| 1913            | 3.13  | 2.29 | 4.68 | 4.52 | 2.50 | 1.02  | 1.64  | 3.62  | 3.13 | 6.46  | 2.18 | 2.47 | 37.64 |
| 1914            | 3.57  | 2.03 | 3.77 | 3.24 | 2.65 | 2.80  | 4.63  | 2.01  | 0.24 | 2.52  | 2.48 | 4.10 | 34.04 |
| 1915            | 4.79  | 4.75 | 0.42 | 1.75 | 2.10 | 2.79  | 6.10  | 7.30  | 2.32 | 2.57  | 1.08 | 5.73 | 41.70 |
| 1916            | 0.98  | 3.34 | 2.66 | 2.71 | 2.62 | 4.87  | 6.50  | 1.99  | 2.49 | 1.04  | 2.65 | 4.09 | 35.94 |
| 1917            | 2.79  | 1.67 | 3.04 | 1.71 | 2.66 | 3.60  | 2.55  | 1.67  | 0.95 | 4.61  | 1.05 | 2.77 | 29.07 |
| 1918            | 3.33  | 2.19 | 1.39 | 4.10 | 3.52 | 3.44  | 4.69  | 3.36  | 3.42 | 1.23  | 2.31 | 3.82 | 36.80 |
| 1919            | 2.70  | 2.96 | 4.46 | 2.66 | 3.99 | 2.03  | 7.17  | 4.40  | 4.21 | 3.17  | 4.01 | 2.55 | 44.31 |
| 1920            | 2.19  | 4.33 | 3.04 | 3.83 | 1.93 | 5.21  | 4.26  | 4.04  | 5.75 | 1.87  | 3.04 | 4.32 | 43.81 |
| 1921            | 2.10  | 2.95 | 2.76 | 4.94 | 2.07 | 3.38  | 4.33  | 2.81  | 2.60 | 1.05  | 3.72 | 2.04 | 34.75 |
| 1922            | 1.12  | 2.35 | 3.54 | 2.40 | 4.64 | 6.49  | 5.68  | 3.47  | 2.02 | 1.88  | 0.97 | 3.20 | 37.76 |
| 1923            | 4.22  | 1.87 | 2.43 | 2.98 | 2.33 | 3.32  | 3.07  | 1.82  | 2.87 | 3.87  | 3.90 | 3.44 | 36.12 |
| 1924            | 3.60  | 2.46 | 0.90 | 5.35 | 4.60 | 1.79  | 1.94  | 2.34  | 4.38 | 0.44  | 2.12 | 1.66 | 31.58 |
| 1925            | 3.75  | 2.61 | 3.30 | 1.74 | 2.57 | 4.13  | 7.10  | 1.76  | 2.97 | 3.52  | 3.39 | 2.43 | 39.27 |
| 1926            | 1.82  | 3.91 | 1.77 | 2.47 | 1.50 | 2.34  | 3.62  | 4.66  | 2.71 | 3.78  | 3.08 | 2.54 | 34.20 |
| 1927            | 2.17  | 2.51 | 1.40 | 2.20 | 5.15 | 2.80  | 4.08  | 6.59  | 2.89 | 5.57  | 7.14 | 4.34 | 46.84 |
| 1928            | 2.05  | 3.86 | 2.11 | 4.52 | 2.32 | 7.06  | 7.92  | 8.27  | 2.64 | 0.75  | 2.26 | 1.09 | 44.85 |
| 1929            | 3.18  | 3.14 | 2.14 | 6.55 | 3.25 | 1.82  | 2.67  | 3.02  | 2.73 | 3.61  | 2.43 | 3.69 | 38.23 |
| 1930            | 2.13  | 1.80 | 2.28 | 2.07 | 3.04 | 4.22  | 2.72  | 3.48  | 2.22 | 1.20  | 3.65 | 2.57 | 31.38 |
| 1931            | 1.39  | 1.77 | 2.60 | 3.07 | 4.93 | 5.91  | 6.55  | 3.73  | 1.46 | 1.82  | 1.31 | 2.44 | 36.98 |
| 1932            | 3.00  | 1.83 | 3.24 | 1.79 | 3.09 | 3.01  | 4.24  | 4.34  | 1.65 | 5.60  | 7.27 | 1.76 | 40.82 |
| 1933            | 1.31  | 2.56 | 4.04 | 4.52 | 2.09 | 2.70  | 2.31  | 9.25  | 5.48 | 2.10  | 0.99 | 2.23 | 39.58 |
| 1934            | 2.36  | 2.14 | 2.74 | 3.93 | 4.31 | 3.62  | 5.44  | 2.75  | 8.14 | 2.20  | 4.25 | 2.22 | 44.10 |
| 1935            | 3.32  | 2.45 | 1.84 | 3.08 | 1.79 | 3.45  | 3.56  | 1.29  | 2.92 | 2.35  | 4.83 | 1.09 | 31.97 |
| 1936            | 3.94  | 2.86 | 4.99 | 3.38 | 2.48 | 3.38  | 4.34  | 6.99  | 3.13 | 3.19  | 1.71 | 4.66 | 45.05 |
| 1937            | 6.42  | 1.86 | 2.73 | 4.51 | 4.08 | 6.38  | 2.95  | 3.91  | 3.11 | 2.96  | 2.92 | 2.32 | 44.15 |
| 1938            | 2.95  | 1.55 | 1.61 | 2.06 | 4.39 | 5.95  | 7.08  | 5.97  | 9.85 | 1.83  | 2.24 | 2.51 | 47.99 |
| 1939            | 2.26  | 3.78 | 2.75 | 4.28 | 1.18 | 2.48  | 2.70  | 2.04  | 2.24 | 4.27  | 1.32 | 1.22 | 30.52 |
| 1940            | 0.98  | 2.01 | 3.66 | 4.69 | 5.58 | 3.33  | 4.45  | 3.13  | 2.64 | 2.00  | 4.35 | 2.88 | 39.70 |
| 1941            | 2.17  | 2.22 | 0.95 | 0.78 | 1.64 | 4.80  | 5.01  | 2.39  | 0.87 | 1.78  | 1.92 | 2.64 | 27.17 |
| 1942            | 2.76  | 1.81 | 4.98 | 0.87 | 2.79 | 2.68  | 4.03  | 4.37  | 3.40 | 3.87  | 4.54 | 4.59 | 40.69 |
| 1943            | 2.67  | 1.56 | 2.58 | 3.14 | 5.51 | 4.46  | 6.47  | 1.10  | 1.73 | 6.67  | 3.70 | 0.51 | 40.10 |
| 1944            | 0.98  | 1.33 | 4.22 | 3.28 | 1.79 | 5.08  | 3.50  | 0.61  | 4.87 | 1.45  | 4.88 | 2.98 | 34.97 |
| 1945            | 4.06  | 3.50 | 1.89 | 4.77 | 7.49 | 5.82  | 10.77 | 5.73  | 5.60 | 2.40  | 4.41 | 3.81 | 60.25 |
| 1946            | 1.14  | 2.62 | 1.58 | 1.50 | 4.61 | 2.93  | 5.97  | 2.95  | 3.68 | 1.42  | 0.76 | 2.12 | 31.28 |
| 1947            | 2.53  | 1.84 | 2.39 | 4.30 | 5.06 | 4.32  | 4.36  | 3.24  | 2.85 | 2.43  | 6.09 | 3.18 | 42.59 |
| 1948            | 3.06  | 1.92 | 3.12 | 4.57 | 4.41 | 4.34  | 2.10  | 2.35  | 0.78 | 1.99  | 3.85 | 7.40 | 39.89 |
| 1949            | 4.69  | 2.48 | 1.19 | 2.37 | 4.60 | 0.99  | 3.19  | 4.26  | 2.54 | 2.34  | 1.90 | 4.03 | 34.58 |
| 1950            | 3.79  | 3.01 | 2.80 | 2.42 | 4.34 | 4.02  | 4.12  | 3.68  | 2.29 | 1.24  | 5.69 | 3.09 | 40.49 |
| 1951            | 3.30  | 3.28 | 5.07 | 2.89 | 3.78 | 3.52  | 3.53  | 5.87  | 3.17 | 3.62  | 5.26 | 3.50 | 46.79 |
| 1952            | 4.01  | 1.69 | 3.28 | 7.41 | 5.33 | 4.96  | 4.32  | 5.87  | 4.73 | 0.85  | 2.35 | 3.69 | 48.49 |
| 1953            | 4.09  | 2.23 | 6.63 | 5.58 | 5.22 | 3.15  | 2.52  | 2.19  | 2.33 | 4.31  | 1.86 | 4.64 | 44.75 |
| 1954            | 1.52  | 1.88 | 3.07 | 2.97 | 4.57 | 1.57  | 2.09  | 5.18  | 5.48 | 1.45  | 6.77 | 3.27 | 39.82 |
| 1955            | 0.79  | 2.85 | 4.38 | 3.62 | 1.75 | 2.37  | 0.82  | 12.71 | 2.59 | 10.40 | 4.42 | 0.54 | 47.24 |
| 1956            | 1.84  | 3.63 | 3.71 | 4.41 | 2.78 | 1.68  | 4.36  | 1.72  | 6.30 | 2.49  | 1.72 | 4.25 | 38.89 |
| 1957            | 1.80  | 1.15 | 2.13 | 4.60 | 2.94 | 1.19  | 2.23  | 1.66  | 2.29 | 3.11  | 3.05 | 5.71 | 31.86 |
| 1958            | 4.32  | 2.54 | 3.60 | 6.01 | 3.85 | 1.82  | 2.92  | 2.20  | 3.95 | 5.04  | 3.73 | 0.62 | 40.60 |
| 1959            | 2.92  | 2.56 | 2.43 | 3.01 | 1.83 | 3.58  | 3.98  | 3.56  | 0.72 | 6.81  | 3.26 | 2.93 | 37.59 |
| 1960            | 2.34  | 2.81 | 1.71 | 3.13 | 3.51 | 4.75  | 5.65  | 2.28  | 6.08 | 2.21  | 1.76 | 1.63 | 37.86 |
| 1961            | 2.35  | 3.47 | 3.08 | 4.78 | 4.10 | 3.14  | 2.96  | 1.99  | 2.52 | 1.54  | 4.12 | 2.69 | 36.74 |
| 1962            | 3.03  | 5.20 | 1.11 | 2.94 | 1.36 | 2.82  | 1.43  | 3.85  | 1.91 | 2.59  | 2.33 | 2.99 | 31.56 |
| 1963            | 2.69  | 2.18 | 2.57 | 1.04 | 1.36 | 4.32  | 4.16  | 1.81  | 3.12 | 0.36  | 5.36 | 2.22 | 31.19 |
| 1964            | 2.12  | 1.79 | 2.26 | 3.41 | 0.94 | 2.98  | 1.99  | 2.35  | 1.30 | 0.89  | 1.67 | 2.82 | 24.52 |
| 1965            | 2.24  | 2.24 | 1.13 | 2.40 | 1.05 | 1.54  | 2.91  | 4.38  | 2.66 | 2.92  | 2.16 | 2.08 | 27.71 |
| 1966            | 1.89  | 2.21 | 1.99 | 2.20 | 3.13 | 1.04  | 0.96  | 0.87  | 6.86 | 4.49  | 3.14 | 2.23 | 31.01 |
| 1967            | 1.23  | 1.52 | 4.44 | 3.44 | 2.91 | 7.23  | 5.32  | 5.76  | 1.48 | 2.92  | 2.54 | 4.16 | 42.95 |
| 1968            | 1.20  | 0.72 | 3.86 | 2.37 | 6.50 | 5.57  | 0.72  | 2.05  | 3.83 | 2.16  | 3.88 | 3.87 | 36.73 |

Table No. 6A

Historical Precipitation at Station KPOU  
Poughkeepsie, NY

| Precip.<br>(in)     | Month |      |      |      |       |       |       |       |      |       |      |      | TOTAL        |
|---------------------|-------|------|------|------|-------|-------|-------|-------|------|-------|------|------|--------------|
|                     | J     | F    | M    | A    | M     | J     | J     | A     | S    | O     | N    | D    |              |
| 1969                | 1.45  | 1.85 | 2.51 | 4.21 | 3.27  | 4.16  | 5.06  | 3.60  | 3.25 | 1.56  | 6.41 | 4.15 | 41.48        |
| 1970                | 0.43  | 2.97 | 2.01 | 3.82 | 2.96  | 2.96  | 1.89  | 4.03  | 3.31 | 2.93  | 3.96 | 3.10 | 34.37        |
| 1971                | 1.68  | 3.58 | 1.99 | 2.62 | 5.03  | 1.47  | 5.22  | 10.92 | 3.98 | 3.51  | 3.41 | 2.70 | 46.11        |
| 1972                | 2.23  | 3.53 | 3.22 | 4.75 | 7.74  | 7.99  | 4.13  | 2.14  | 1.93 | 3.68  | 8.11 | 5.33 | 54.78        |
| 1973                | 2.81  | 1.82 | 3.83 | 6.50 | 6.17  | 4.89  | 2.43  | 1.24  | 2.71 | 1.61  | 1.76 | 8.65 | 44.42        |
| 1974                | 4.20  | 1.12 | 3.86 | 3.94 | 4.46  | 4.65  | 4.25  | 3.82  | 5.20 | 2.55  | 2.82 | 3.08 | 43.95        |
| 1975                | 3.51  | 3.11 | 3.99 | 1.88 | 3.14  | 3.99  | 13.63 | 3.15  | 7.19 | 4.31  | 4.35 | 2.98 | 55.23        |
| 1976                | 3.67  | 2.76 | 1.79 | 2.28 | 3.36  | 2.67  | 5.10  | 7.27  | 3.90 | 6.78  | 0.67 | 2.09 | 42.34        |
| 1977                | 1.27  | 3.33 | 6.11 | 4.17 | 2.59  | 3.38  | 1.43  | 3.24  | 5.95 | 4.72  | 5.25 | 4.45 | 45.89        |
| 1978                | 7.09  | 1.13 | 3.38 | 1.08 | 7.08  | 3.29  | 2.83  | 4.14  | 2.76 | 1.97  | 1.70 | 3.38 | 39.83        |
| 1979                | 6.65  | 3.09 | 2.05 | 3.95 | 5.82  | 1.62  | 2.10  | 4.32  | 5.71 | 4.02  | 3.50 | 1.85 | 44.68        |
| 1980                | 0.64  | 0.92 | 4.55 | 5.18 | 1.86  | 3.62  | 2.79  | 2.50  | 1.83 | 3.15  | 3.07 | 0.57 | 30.68        |
| 1981                | 0.77  | 5.42 | 0.15 | 4.01 | 4.82  | 3.81  | 3.79  | 0.64  | 2.81 | 4.12  | 1.28 | 3.61 | 35.23        |
| 1982                | 3.76  | 3.15 | 2.78 | 3.63 | 2.97  | 8.39  | 3.58  | 3.86  | 2.14 | 1.60  | 3.00 | 0.93 | 39.79        |
| 1983                | 3.72  | 2.23 | 7.39 | 8.51 | 6.84  | 4.03  | 1.28  | 4.00  | 2.36 | 3.57  | 4.91 | 6.60 | 55.44        |
| 1984                | 1.33  | 3.37 | 3.70 | 5.14 | 11.49 | 1.58  | 5.53  | 1.90  | 0.84 | 2.20  | 2.04 | 2.65 | 41.77        |
| 1985                | 1.00  | 2.04 | 2.58 | 1.71 | 4.19  | 3.34  | 4.66  | 4.68  | 5.31 | 1.72  | 6.11 | 2.23 | 39.57        |
| 1986                | 3.48  | 3.52 | 2.96 | 1.68 | 2.10  | 5.87  | 9.00  | 2.84  | 0.46 | 2.51  | 5.23 | 3.28 | 42.93        |
| 1987                | 3.65  | 0.32 | 3.12 | 6.47 | 2.22  | 2.35  | 4.51  | 3.79  | 6.59 | 4.70  | 1.27 | 1.50 | 40.49        |
| 1988                | 2.11  | 2.97 | 1.61 | 1.36 | 4.51  | 0.30  | 8.49  | 4.54  | 1.93 | 1.50  | 7.10 | 0.88 | 37.30        |
| 1989                | 1.72  | 2.29 | 3.00 | 2.78 | 11.81 | 7.21  | 1.63  | 3.63  | 6.71 | 6.54  | 1.86 | 1.01 | 50.19        |
| 1990                | 4.10  | 3.49 | 3.25 | 3.05 | 6.04  | 3.28  | 3.30  | 7.91  | 1.19 | 5.85  | 2.70 | 5.00 | 49.16        |
| 1991                | 1.50  | 1.63 | 3.82 | 3.58 | 5.05  | 2.21  | 2.72  | 4.92  | 4.81 | 4.07  | 3.70 | 3.03 | 41.04        |
| 1992                | 1.70  | 1.92 | 3.08 | 3.12 | 2.83  | 3.34  | 7.18  | 2.81  | 1.98 | 1.31  | 4.60 | 4.16 | 38.03        |
| 1993                | 2.28  | 2.70 | 5.69 | 5.17 | 1.07  | 2.71  | 1.32  | 1.95  | 6.05 | 3.82  | 3.46 | 3.62 | 39.84        |
| 1994                | 3.69  | 2.86 | 5.25 | 3.06 | 3.63  | 5.62  | 5.12  | 5.97  | 3.03 | 1.23  | 3.56 | 2.67 | 45.69        |
| 1995                | 4.49  | 2.52 | 2.53 | 3.76 | 3.51  | 2.34  | 11.27 | 1.80  | 3.30 | 9.98  | 5.40 | 2.62 | 53.52        |
| 1996                | 7.41  | 2.21 | 3.26 | 6.56 | 3.71  | 4.06  | 11.62 | 1.39  | 5.94 | 7.48  | 2.58 | 7.09 | 63.31        |
| 1997                | 2.68  | 1.47 | 4.11 | 4.86 | 5.15  | 2.24  | 4.29  | 4.52  | 2.70 | 1.83  | 6.01 | 3.50 | 43.36        |
| 1998                | 3.72  | 2.54 | 4.17 | 4.26 | 6.33  | 10.79 | 2.23  | 2.67  | 3.78 | 3.74  | 1.39 | 1.06 | 46.68        |
| 1999                | 6.16  | 2.53 | 5.36 | 1.57 | 3.38  | 1.50  | 2.11  | 4.22  | 6.94 | 3.47  | 2.40 | 2.08 | 41.72        |
| 2000                | 2.95  | 3.31 | 4.58 | 4.90 | 8.10  | 7.02  | 4.23  | 5.28  | 3.70 | 1.77  | 2.63 | 4.27 | 52.74        |
| 2001                | 2.18  | 2.25 | 6.37 | 0.11 | 2.69  | 4.64  | 2.85  | 3.24  | 4.76 | 0.79  | 0.85 | 2.08 | 32.81        |
| 2002                | 1.03  | 0.87 | 2.39 | 3.96 | 4.51  | 4.12  | 3.84  | 4.05  | 2.74 | 5.63  | 5.18 | 2.91 | 41.23        |
| 2003                | 2.58  | 2.56 | 3.08 | 1.47 | 3.78  | 4.47  | 2.44  | 4.31  | 9.22 | 4.34  | 4.31 | 3.98 | 46.54        |
| 2004                | 1.95  | 1.86 | 1.87 | 2.92 | 2.27  | 1.74  | 4.94  | 6.23  | 8.14 | 1.8   | 2.93 | 3.48 | 40.13        |
| 2005                | 4.79  | 1.58 | 3.88 | 3.78 | 1.95  | 4.7   | 7.78  | 2.01  | 0.61 | 17.59 | 4.68 | 3.57 | 56.92        |
| 2006                | 5.76  | 1.03 | 0.7  | 3.95 | 7.68  | 6.49  | 1.68  | 5.06  | 4.93 | 4.21  | 4.9  |      | 46.39        |
| <b>1896 to 2006</b> |       |      |      |      |       |       |       |       |      |       |      |      |              |
| <b>Mean</b>         | 2.79  | 2.59 | 3.13 | 3.46 | 3.78  | 3.71  | 4.35  | 3.89  | 3.53 | 3.26  | 3.23 | 3.12 | <b>40.81</b> |
| <b>Min.</b>         | 0.43  | 0.32 | 0.15 | 0.11 | 0.74  | 0.30  | 0.72  | 0.61  | 0.24 | 0.36  | 0.63 | 0.51 | 24.52        |
| <b>Max.</b>         | 7.41  | 5.49 | 7.39 | 8.51 | 11.81 | 10.90 | 15.71 | 12.71 | 9.85 | 17.59 | 8.11 | 8.65 | 63.31        |
| <b>Median</b>       | 2.67  | 2.46 | 3.00 | 3.28 | 3.50  | 3.38  | 4.08  | 3.63  | 2.97 | 2.59  | 3.04 | 2.96 | 40.13        |

## Notes:

1. All data from Station KPOU (Poughkeepsie) except for select dates from 1995 through 2001 where data at this station was unavailable. Data from these dates collected from West Point, NY Station or Danbury, CT Station.

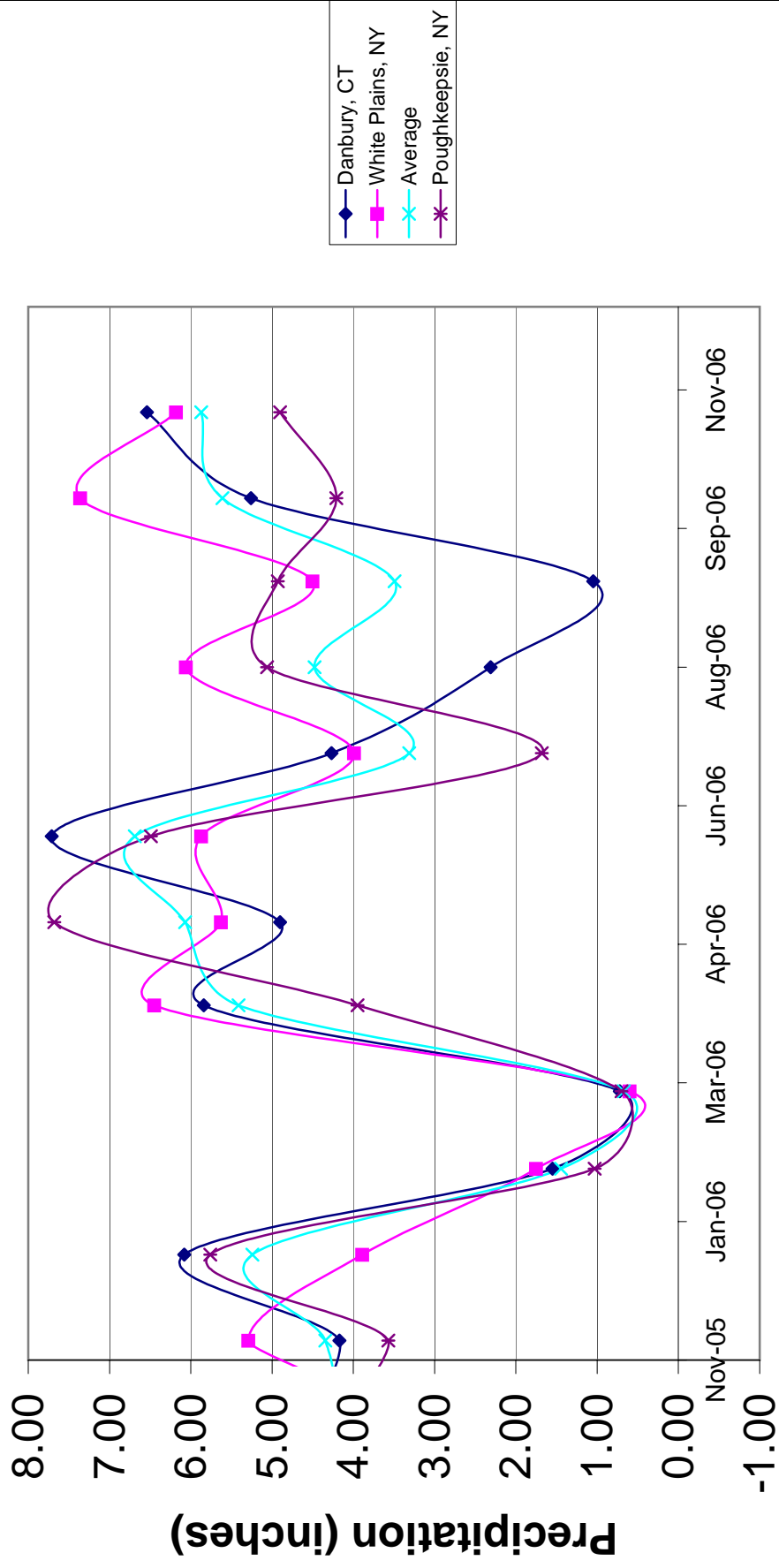


Table No. 6B

## Monthly Precipitation since January 2003

| Month  | Poughkeepsie, NY<br>(KPOU) | Danbury, CT<br>(KDXR) | White Plains, NY<br>(KHPN) | Average      |
|--|----------------------------|-----------------------|----------------------------|--------------|
| Jan-03   | 2.58                       | 2.60                  | 2.07                       | 2.42         |
| Feb-03   | 2.56                       | 2.74                  | 1.15                       | 2.15         |
| Mar-03   | 3.08                       | 3.86                  | 3.90                       | 3.61         |
| Apr-03   | 1.47                       | 2.42                  | 2.84                       | 2.24         |
| May-03   | 3.78                       | 4.33                  | 4.44                       | 4.18         |
| Jun-03   | 4.47                       | 8.87                  | 7.98                       | 7.11         |
| Jul-03   | 2.44                       | 4.07                  | 1.78                       | 2.76         |
| Aug-03   | 4.31                       | 6.83                  | 4.57                       | 5.24         |
| Sep-03   | 9.22                       | 7.99                  | 7.25                       | 8.15         |
| Oct-03   | 4.34                       | 5.03                  | 4.35                       | 4.57         |
| Nov-03   | 4.31                       | 4.11                  | 4.14                       | 4.19         |
| Dec-03   | 3.98                       | 6.19                  | 5.45                       | 5.21         |
| Jan-04   | 1.95                       | 1.57                  | 1.83                       | 1.78         |
| Feb-04   | 1.86                       | 2.21                  | 2.62                       | 2.23         |
| Mar-04   | 1.87                       | 3.33                  | 3.87                       | 3.02         |
| Apr-04   | 2.92                       | 5.31                  | 5.31                       | 4.51         |
| May-04   | 2.27                       | 3.11                  | 3.92                       | 3.10         |
| Jun-04   | 1.74                       | 2.46                  | 3.19                       | 2.46         |
| Jul-04   | 4.94                       | 4.75                  | 7.04                       | 5.58         |
| Aug-04   | 6.23                       | 2.50                  | 3.46                       | 4.06         |
| Sep-04   | 8.14                       | 8.10                  | 11.50                      | 9.25         |
| Oct-04   | 1.80                       | 2.23                  | 1.34                       | 1.79         |
| Nov-04   | 2.93                       | 3.87                  | 3.86                       | 3.55         |
| Dec-04   | 3.48                       | 4.13                  | 3.15                       | 3.59         |
| Jan-05   | 4.79                       | 3.98                  | 3.89                       | 4.22         |
| Feb-05   | 1.58                       | 2.32                  | 2.94                       | 2.28         |
| Mar-05   | 3.88                       | 3.35                  | 3.59                       | 3.61         |
| Apr-05   | 3.78                       | 5.14                  | 4.93                       | 4.62         |
| May-05   | 1.95                       | 2.01                  | 1.32                       | 1.76         |
| Jun-05   | 4.70                       | 2.75                  | 3.81                       | 3.75         |
| Jul-05   | 7.78                       | 3.74                  | 8.60                       | 6.71         |
| Aug-05   | 2.01                       | 0.65                  | 1.93                       | 1.53         |
| Sep-05   | 0.61                       | 1.88                  | 1.36                       | 1.28         |
| Oct-05   | 17.59                      | 15.35                 | 15.58                      | 16.17        |
| Nov-05   | 4.68                       | 4.98                  | 3.91                       | 4.52         |
| Dec-05   | 3.57                       | 4.17                  | 5.29                       | 4.34         |
| Jan-06   | 5.76                       | 6.08                  | 3.89                       | 5.24         |
| Feb-06   | 1.03                       | 1.55                  | 1.75                       | 1.44         |
| Mar-06   | 0.70                       | 0.72                  | 0.60                       | 0.67         |
| Apr-06   | 3.95                       | 5.84                  | 6.45                       | 5.41         |
| May-06   | 7.68                       | 4.90                  | 5.63                       | 6.07         |
| Jun-06   | 6.49                       | 7.71                  | 5.87                       | 6.69         |
| Jul-06   | 1.68                       | 4.27                  | 3.99                       | 3.31         |
| Aug-06   | 5.06                       | 2.31                  | 6.06                       | 4.48         |
| Sep-06   | 4.93                       | 1.05                  | 4.50                       | 3.49         |
| Oct-06   | 4.21                       | 5.26                  | 7.36                       | 5.61         |
| Nov-06   | 4.90                       | 6.54                  | 6.18                       | 5.87         |
|  |                            |                       |                            |              |
|  |                            |                       |                            |              |
|  |                            |                       |                            |              |
|  |                            |                       |                            |              |
| 2003 Annual Total  | 46.54                      | 59.04                 | 49.92                      | 51.83        |
| 2004 Annual Total  | 40.13                      | 43.57                 | 51.09                      | 44.93        |
| 2005 Annual Total  | 56.92                      | 50.32                 | 57.15                      | 54.80        |
| 2006 Annual Total thru Oct.                              | 41.49                      | 39.69                 | 46.10                      | 42.43        |
| <b>April 2006 - Oct. 2006</b>                            | <b>34.00</b>               | <b>31.34</b>          | <b>39.86</b>               | <b>35.07</b> |
| <b>(6 months preceeding<br/>date of Estimated Flows)</b> |                            |                       |                            |              |

**Plot of Selected data from Table 6B  
Monthly Precipitation Since Nov. 2005**



**Time (months)**

## LIMITATIONS



## LIMITATIONS

### Explorations

1. The analyses and conclusions submitted in this report are based in part upon the data obtained from widely spaced subsurface explorations. The nature and extent of variations between these explorations may become evident with further investigation. If such variations appear, it will be necessary to reevaluate the conclusions of this report.
2. The stratification lines on the logs and soil profile described in the text are intended to convey trends in subsurface conditions. The boundaries between strata are approximate and idealized and have been developed by interpretations of widely spaced explorations and samples; actual soil transitions are probably more erratic. For specific information, refer to the boring logs.
3. Water level readings have been made in the drill holes and observation wells at times and under conditions stated on the logs. These data have been reviewed and interpretations made in the text of this report. However, it must be noted that fluctuations in the level of the groundwater and flow rates may occur due to variations in rainfall, temperature and other factors occurring since the time measurements were made.

### Analyses

4. Preliminary one-dimensional calculations were made during this study. Efforts have been made to check the validity of the assumptions for the simulations performed to-date, and in our opinion, the results have been reasonable. However, it is recognized that calculations developed using different methodologies and/or different assumptions could produce different flow patterns. It should also be noted that fluctuations in the flow patterns variations will occur due to changes in rate and sequence of applications of sewage flows, seasonal precipitation and other climatic fluctuations, as well as other factors. Final analyses using additional data including water level readings made during the wet seasons are required to confirm the results included herein.

### Review

5. In the event that any changes in the nature, design or location of the proposed subsurface disposal systems or other proposed site development features affecting groundwater recharge are planned, the preliminary conclusions and recommendations contained in this report shall not be considered valid unless the changes are reviewed and conclusions of this report modified or verified in writing by **GeoDesign, Inc.** It is recommended that this firm be provided the opportunity to perform final design phase studies to confirm the predicted flow rates.

### Uses of Report

6. This report has been prepared for the exclusive use of Camarda Development Company for specific application to the proposed subsurface disposal system at the proposed Stateline Retail Center, U.S. Route 6, Southeast, New York in accordance with generally accepted hydrogeologic practices. No other warranty, express or implied, is made.

